

Tecniche di Diagnosi Automatica dei Guasti

Parte 1

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2

Tecniche di Diagnosi Automatica dei Guasti. Silvio Simani

Lecture Main Topics

- General introduction
 - State-of-the-art review
 - Fault diagnosis nomenclature
- Main methods for fault diagnosis
 - Parameter estimation methods
 - Observer and filter approaches
 - Parity relations
 - Neural networks and fuzzy systems
- Application examples
- Concluding remarks



Programme Details

- Introduction: Course Introduction
- Issues in Model-Based Fault Diagnosis
- Fault Detection and Isolation (FDI) Methods based on Analytical Redundancy
- Model-based Fault Detection Methods
- The Robustness Problem in Fault Detection
- Fault Identification Methods
- Modelling of Faulty Systems

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Programme Details (Cont'd)

- Residual Generation Techniques
- The Residual Generation Problem

- Fault Diagnosis Technique Integration
- Fuzzy Logic for Residual Generation
- Neural Networks in Fault Diagnosis

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Programme Details (Cont'd)

- Output Observers for Robust Residual Generation
- Unknown Input Observer (UIO)
- FDI Schemes Based on UIO and Output Observers
- Kalman Filtering and FDI from Noisy Measurements
- Residual Robustness to Disturbances

- Application Examples

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Annual Meetings on FDI

- IFAC SAFEPROCESS Symposium
- *Symposium on Fault Detection Supervision and Safety for Technical Processes*
 - 1st held in Baden–Baden, Germany in 1991
 - 2nd in Espo, Finland in 1994
 - 3rd at Hull, UK in 1997
 - 4th held in Budapest, Hungary in 2000
 - 5th at Washington DC in July 2003
 - 6th in Beijing, P.R. China, August 2006
 - 7th in Barcelona, Spain, July 2009
 - 8th scheduled in Mexico City, Mexico, August 2012

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Nomenclature

1. *States and Signals*

Fault

An unpermitted deviation of at least one characteristic property or parameter of the system from the acceptable, usual or standard condition.

Failure

A permanent interruption of a system's ability to perform a required function under specified operating conditions.

Malfunction

An intermittent irregularity in the fulfilment of a system's desired function.

Error

A deviation between a measured or computed value of an output variable and its true or theoretically correct one.

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Nomenclature (cont'd)

1. *States and Signals*

Disturbance

An unknown and uncontrolled input acting on a system.

Residual

A fault indicator, based on a deviation between measurements and model-equation-based computations.

Symptom

A change of an observable quantity from normal behaviour.

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Nomenclature (Cont'd)

2. Functions

Fault detection

Determination of faults present in a system and the time of detection.

Fault isolation

Determination of the kind, location and time of detection of a fault. Follows fault detection.

Fault identification

Determination of the size and time-variant behaviour of a fault. Follows fault isolation.

Fault diagnosis

Determination of the kind, size, location and time of detection of a fault. Follows fault detection. Includes fault detection and identification.

Monitoring

A continuous real-time task of determining the conditions of a physical system, by recording information, recognising and indication anomalies in the behaviour.

Supervision

Monitoring a physical and taking appropriate actions to maintain the operation in the case of fault.

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Nomenclature (Cont'd)

3. Models

Quantitative model

Use of static and dynamic relations among system variables and parameters in order to describe a system's behaviour in quantitative mathematical terms.

Qualitative model

Use of static and dynamic relations among system variables in order to describe a system's behaviour in qualitative terms such as causalities and IF-THEN rules.

Diagnostic model

A set of static or dynamic relations which link specific input variables, *the symptoms*, to specific output variables, the faults.

Analytical redundancy

Use of more (not necessarily identical) ways to determine a variable, where one way uses a mathematical process model in analytical form.

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Nomenclature (Cont'd)

Reliability

Ability of a system to perform a required function under stated conditions, within a given scope, during a given period of time.

Safety

Ability of a system not to cause danger to persons or equipment or the environment.

Availability

Probability that a system or equipment will operate satisfactorily and effectively at any point of time.

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Nomenclature (Cont'd)

5. *Time dependency of faults*

Abrupt fault

Fault modelled as stepwise function. It represents bias in the monitored signal.

Incipient fault

Fault modelled by using ramp signals. It represents drift of the monitored signal.

Intermittent fault

Combination of impulses with different amplitudes.

NOTE: Incipient fault (slowly developing fault) = hard to detect !!!

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Nomenclature (Cont'd)

6. *Fault terminology*

Additive fault

Influences a variable by an addition of the fault itself. They may represent, *e.g.*, offsets of sensors.

Multiplicative fault

Are represented by the product of a variable with the fault itself. They can appear as parameter changes within a process.

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Application Examples

- **Simulated case studies**
- **Identification/FDI applications**
- **Real processes**
- **Research works**
- **Undergraduate theses topics**

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Simulated Application Examples

Simulated Gas Turbine

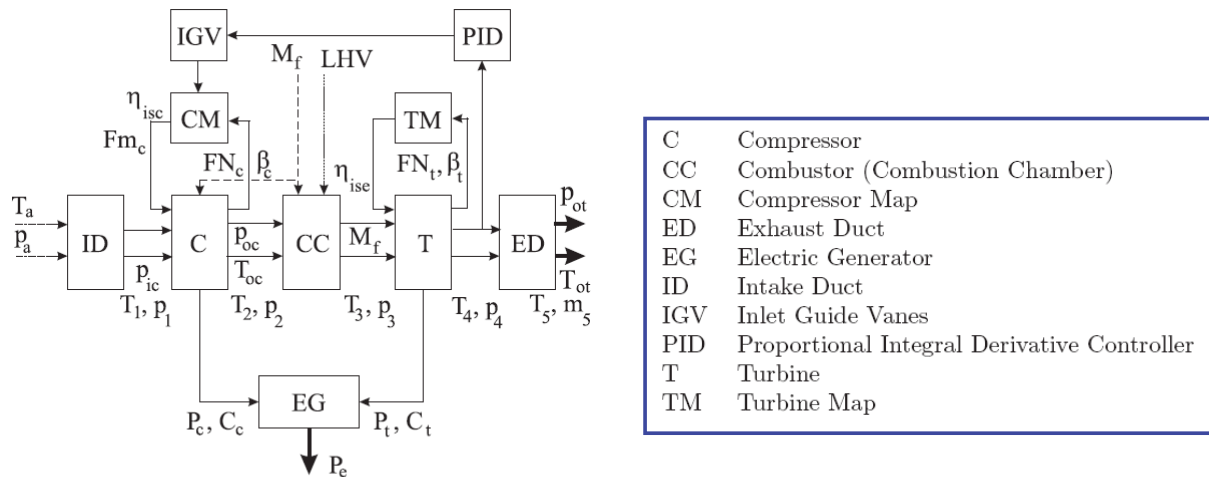


Figure 5.2: Block diagram of the single-shaft gas turbine.

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Simulated Application Examples (Cont'd)

Simulated Gas Turbine

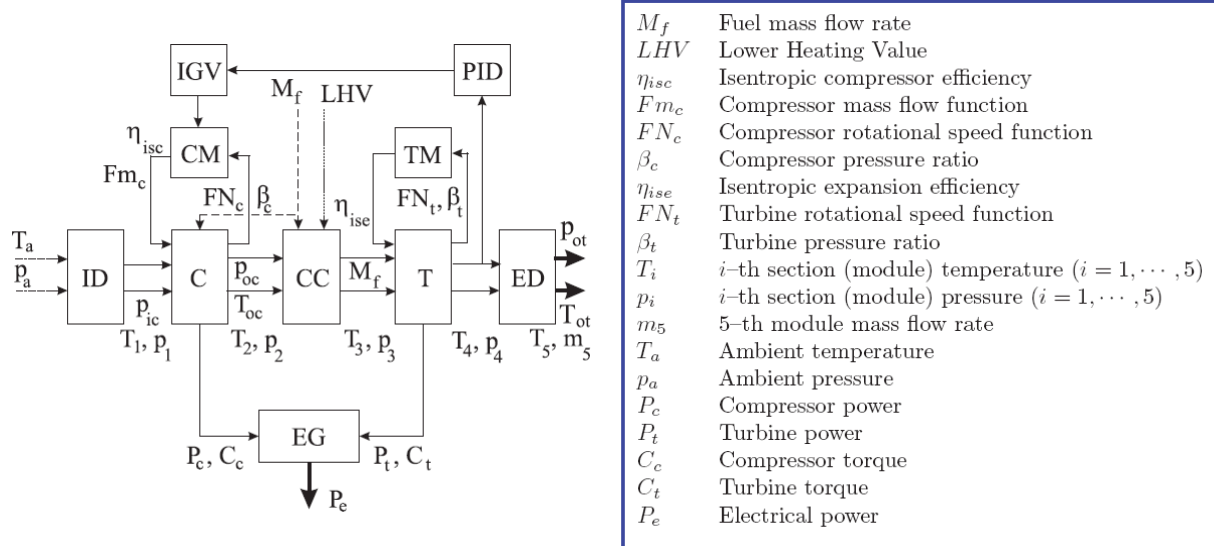
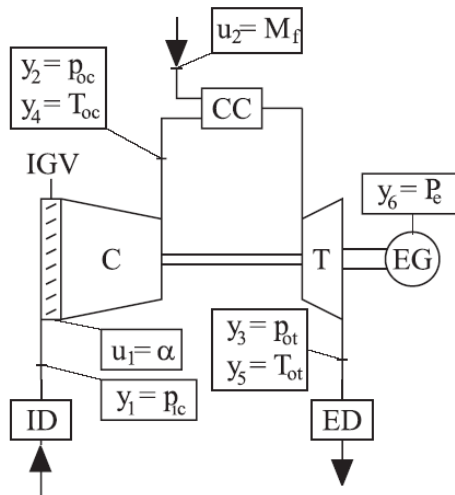


Figure 5.2: Block diagram of the single-shaft gas turbine.

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Simulated Application Examples (Cont'd)

Simulated Gas Turbine



$u_1(t)$, Inlet Guide Vane (IGV) angular position (α);

$u_2(t)$, fuel mass flow rate (M_f).

$y_1(t)$, pressure at the compressor inlet (p_{ic});

$y_2(t)$, pressure at the compressor outlet (p_{oc});

$y_3(t)$, pressure at the turbine outlet (p_{ot});

$y_4(t)$, temperature at the compressor outlet (T_{oc});

$y_5(t)$, temperature at the turbine outlet (T_{ot});

$y_6(t)$, electrical power at the generator terminal (P_e).

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Simulated Application Examples (Cont'd)

Simulated Gas Turbine (SIMULINK®)

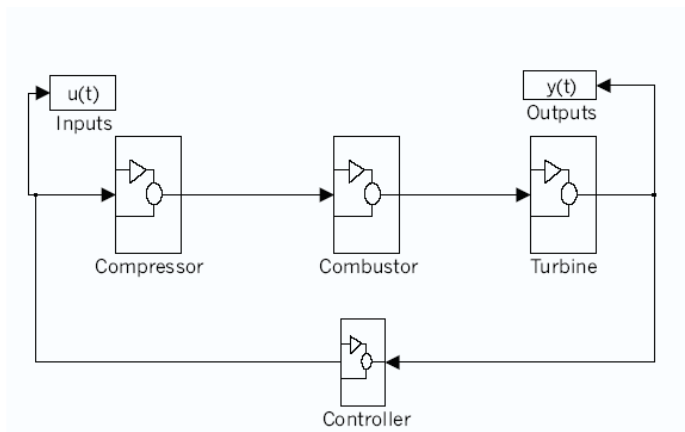


Figure 5.7: SIMULINK block diagram of the process.

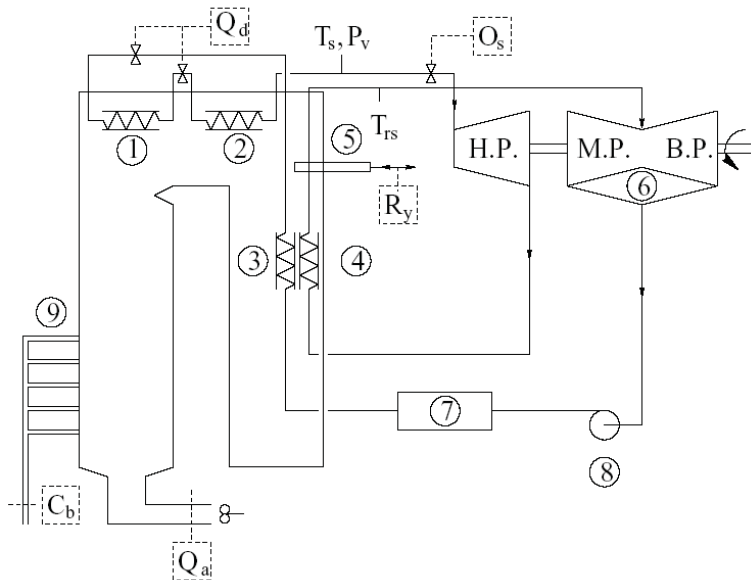
Gas turbine main cycle parameters (ISO design conditions).

Air mass flow rate [kg/s]	24.4
Cycle pressure ratio (P_{oc}/P_{ic})	9.1
Electrical power (P_e) [kW]	5220
Exhaust temperature (T_{ot}) [K]	796
Fuel mass flow rate (M_f) [kg/s]	0.388
IGV angle range ($\Delta\alpha$) [deg]	17

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Simulated Application Examples (Cont'd)

Simulated Power Plant: *Pont sur Sambre*

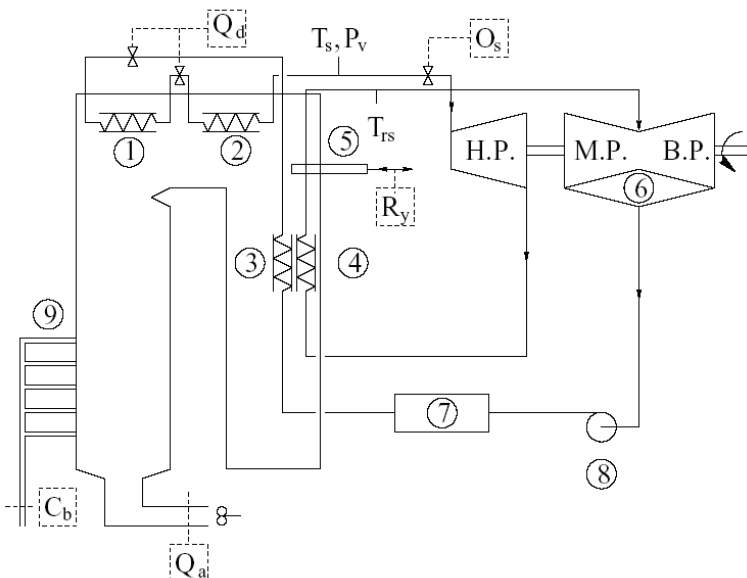


1. super heater (radiation);
2. super heater (convection);
3. super heater;
4. reheater;
5. dampers;
6. condenser;
7. drum;
8. water pump;
9. burner.

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Simulated Application Examples (Cont'd)

Simulated Power Plant: *Pont sur Sambre*



$u_1(t)$	C_b	gas flow
$u_2(t)$	O_s	turbine valves opening
$u_3(t)$	Q_d	super heater spray flow
$u_4(t)$	R_y	gas dampers
$u_4(t)$	Q_a	air flow
$y_1(t)$	P_v	steam pressure
$y_2(t)$	T_s	main steam temperature
$y_i(t)$	T_{rs}	reheat steam temperature

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Simulated Application Examples (Cont'd)

Simulated Gas Turbine

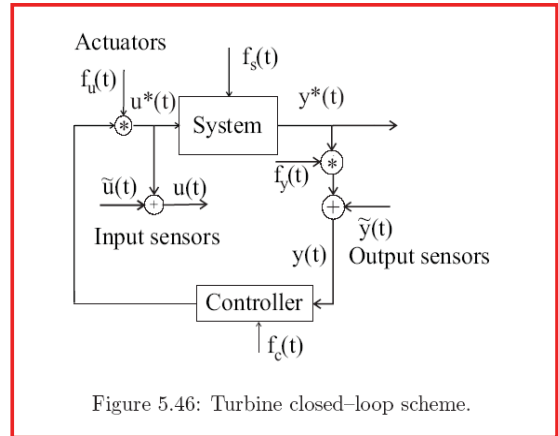
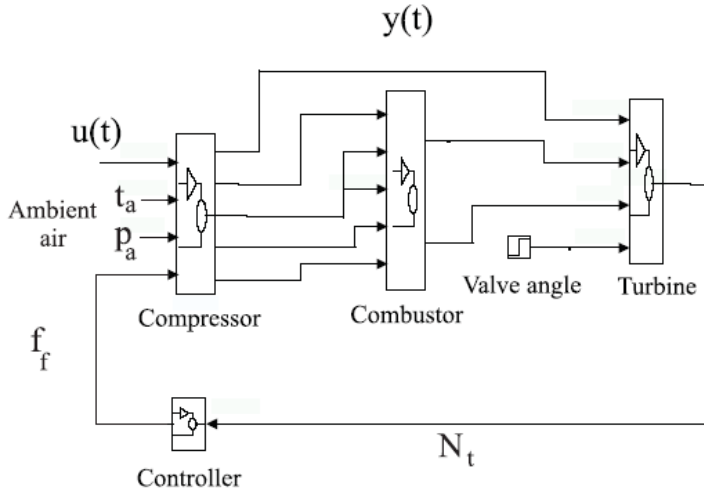


Figure 5.46: Turbine closed-loop scheme.

Figure 5.44: The monitored system.

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Simulated Application Examples (Cont'd)

Small Aircraft Model



Table 1: Nomenclature

V	True Air Speed (TAS)	H	altitude
α	angle of attack	δ_e	elevator deflection angle
β	angle of sideslip	δ_a	aileron deflection angle
P	roll rate	δ_r	rudder deflection angle
Q	pitch rate	δ_{th}	throttle aperture percentage
R	yaw rate	γ	flight path angle
ϕ	bank angle	g	acceleration of gravity
θ	elevation angle	m	airplane mass
ψ	heading angle	I_x, I_y, I_z	principal-axis inertia moments
n	engine shaft angular rate	d_t	distance of c.g. from the Thrust line

Piper Malibu

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Simulated Application Examples (Cont'd)

Small Aircraft Model



Table 1: Nomenclature

V	True Air Speed (TAS)	H	altitude
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n	engine shaft angular rate	d_t	distance of c.g. from the Thrust line

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Simulated Application Examples (Cont'd)

6.1 SATELLITE OVERVIEW

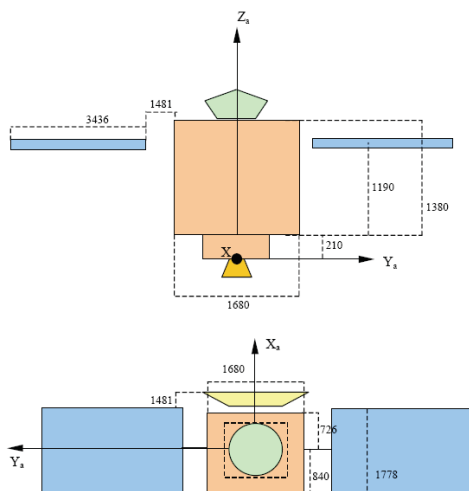


Figure 6-1: Satellite dimensions

6.4 SOLAR ARRAYS DYNAMICS

A GLOBALSTAR solar array has been selected. Its dimensions are recalled on the Figure 6-2.

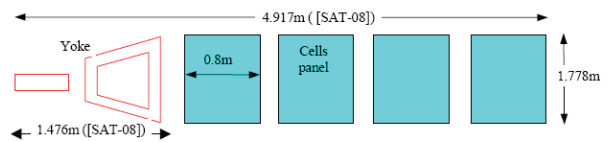


Figure 6-2: MARS-EXPRESS solar array

Simple SA model

Aerospace Satellite

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Simulated Application Examples (Cont'd)

Aerospace Satellite

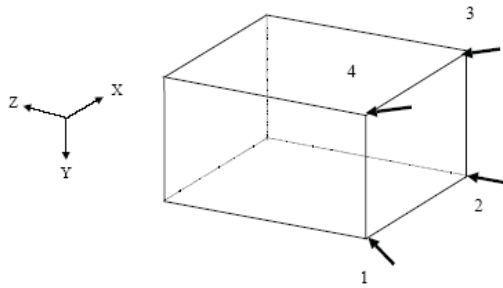


Figure 6-3: Thrusters implementation

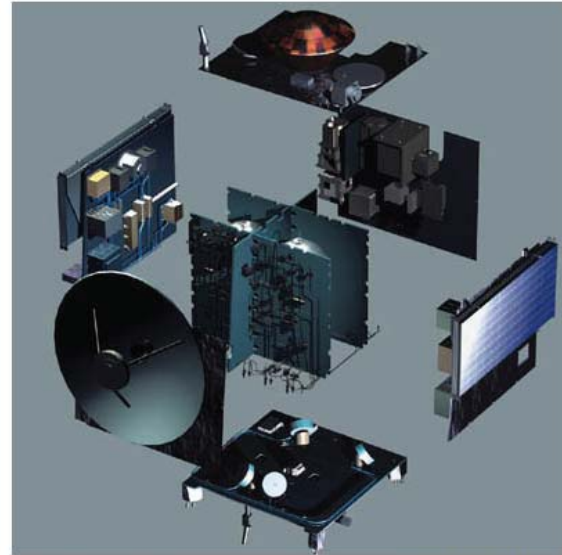
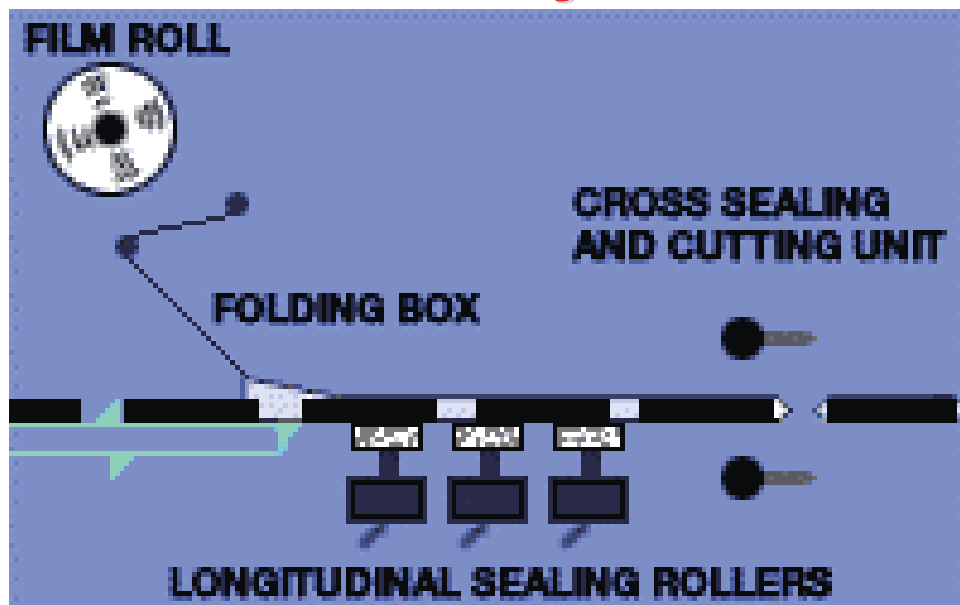


Fig. 1: Mars Express spacecraft (MEX) (www.esa.int)

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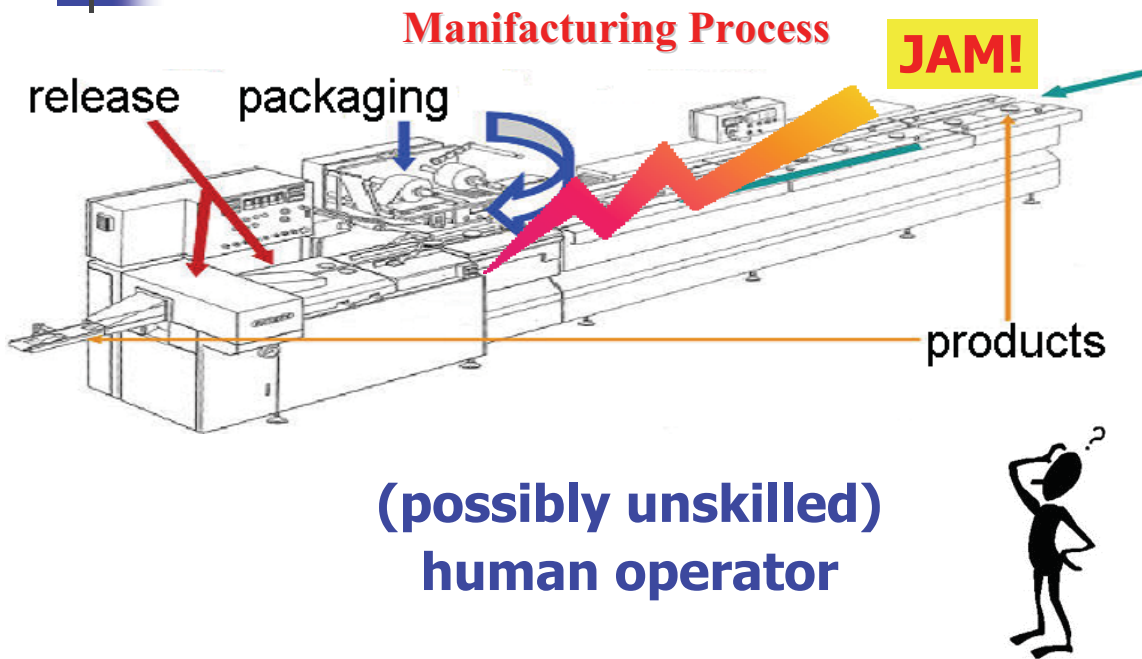
Simulated Application Examples (Cont'd)

Manufacturing Process



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Simulated Application Examples (Cont'd)



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Introduction

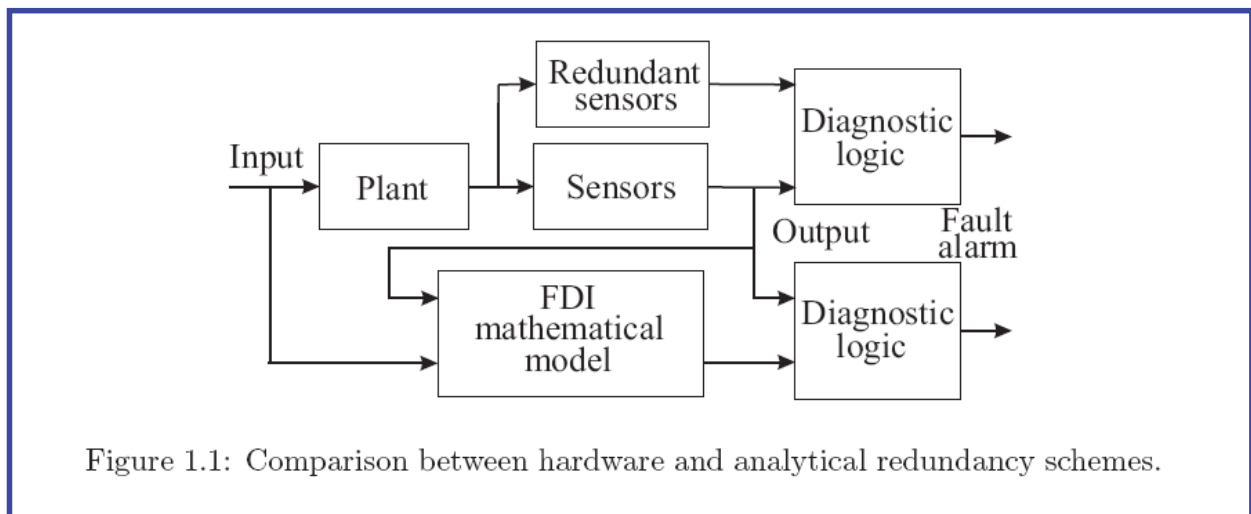


Figure 1.1: Comparison between hardware and analytical redundancy schemes.

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Introduction (Cont'd)

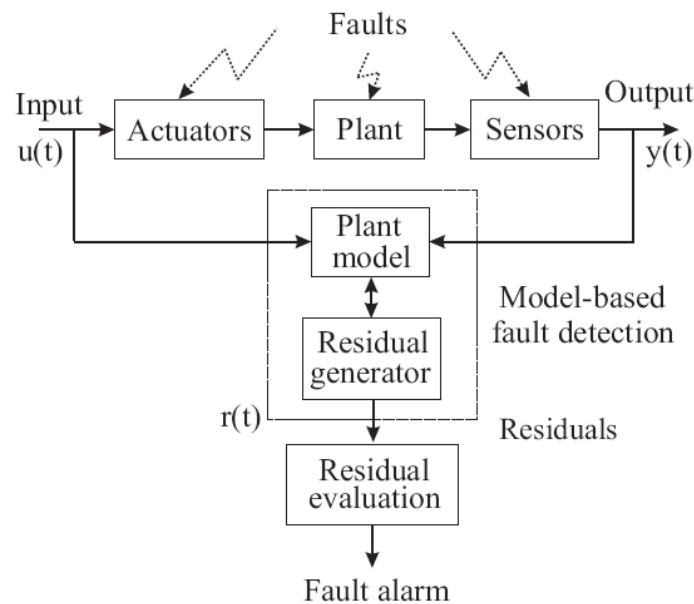


Figure 1.2: Scheme for the model-based fault detection.

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Residual Generation

- This block generates residual signals using available inputs and outputs from the monitored system
- This residual (or fault symptom) should indicate that a fault has occurred
- Normally zero or close to zero under no fault condition, whilst distinguishably different from zero when a fault occurs

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Residual Evaluation

- This block examines residuals for the likelihood of faults and a decision rule is then applied to determine if any faults have occurred
- It may perform a simple threshold test (geometrical methods) on the instantaneous values or moving averages of the residuals
- It may consist of statistical methods, e.g., generalised likelihood ratio testing or sequential probability ratio testing

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Introduction (Cont'd)

- **Model-Based FDI Methods:**

1. Output observers (OO, estimators, filters);
2. Parity equations;
3. Identification and parameter estimation.

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Introduction (Cont'd)

■ Signal Model-Based Methods:

1. Bandpass filters;
2. Spectral analysis (FFT);
3. Maximum-entropy estimation.

■ Change Detection: Residual Analysis

1. Mean and variance estimation;
2. Likelihood-ratio test, Bayes decision;
3. Run-sum test.

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Introduction (Cont'd)

- Model Uncertainty and FDI
 - Model-reality mismatch
 - Sensitivity problem: incipient faults!
- Robustness in FDI
 - Disturbance, modelling errors, uncertainty
 - UIO and Kalman filter: robust residual generation
- System Identification for FDI
 - Estimation of a reliable model
 - Modelling accuracy
 - Disturbance estimation (recall: ARX, ARMAX, BJ)

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Introduction (Cont'd)

■ Fault Identification Methods

■ Fault nature (type, shape) & size (amplitude)

1. Geometrical distance and probabilistic methods;
2. Artificial neural networks;
3. Fuzzy clustering.

■ Approximate Reasoning Methods:

1. Probabilistic reasoning;
2. Possibilistic reasoning with fuzzy logic;
3. Reasoning with artificial neural networks.

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Introduction (Cont'd)

■ FDI applications status & review

Table 1.1: FDI applications and number of contributions.

Application	Number of contributions
Simulation of real processes	55
Large-scale pilot processes	44
Small-scale laboratory processes	18
Full-scale industrial processes	48

Table 1.2: Fault type and number of contributions.

Fault type	Number of contributions
Sensor faults	69
Actuator faults	51
Process faults	83
Control loop or controller faults	8

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Introduction (Cont'd)

■ FDI applications status & review

Table 1.3: FDI methods and number of contributions.

Method type	Number of contributions
Observer	53
Parity space	14
Parameter estimation	51
Frequency spectral analysis	7
Neural networks	9

Table 1.4: Residual evaluation methods and number of contributions.

Evaluation method	Number of contributions
Neural networks	19
Fuzzy logic	5
Bayes classification	4
Hypothesis testing	8

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Introduction (Cont'd)

■ FDI applications status & review

Table 1.5: Reasoning strategies and number of contributions.

Reasoning strategy	Number of contributions
Rule based	10
Sign directed graph	3
Fault symptom tree	2
Fuzzy logic	6

Table 1.6: Applications of model-based fault detection.

FDD	Number of contributions
Milling and grinding processes	41
Power plants and thermal processes	46
Fluid dynamic processes	17
Combustion engine and turbines	36
Automotive	8
Inverted pendulum	33
Miscellaneous	42
DC motors	61
Stirred tank reactor	27
Navigation system	25
Nuclear process	10

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Model-based FDI Techniques

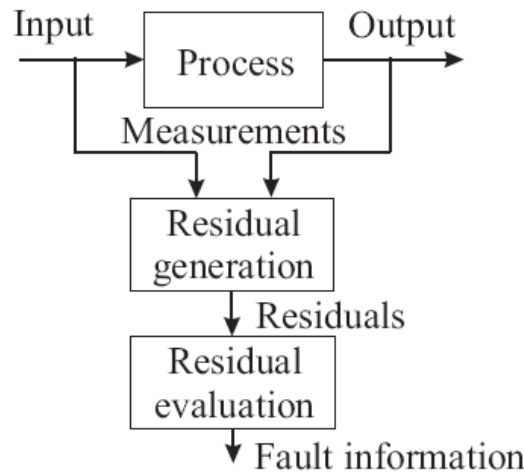


Figure 2.1: Structure of model-based FDI system.

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Model-based FDI Techniques (Cont'd)

1. **Residual generation:** this block generates residual signals using available inputs and outputs from the monitored system. This residual (or fault symptom) should indicate that a fault has occurred. It should normally be zero or close to zero under no fault condition, whilst distinguishably different from zero when a fault occurs. This means that the residual is characteristically independent of process inputs and outputs, in ideal conditions. Referring to Figure 2.1, this block is called *residual generation*.
2. **Residual evaluation:** This block examines residuals for the likelihood of faults and a decision rule is then applied to determine if any faults have occurred. The *residual evaluation* block, shown in Figure 2.1, may perform a simple threshold test (geometrical methods) on the instantaneous values or moving averages of the residuals. On the other hand, it may consist of statistical methods, *e.g.*, generalised likelihood ratio testing or sequential probability ratio testing [Isermann, 1997, Willsky, 1976, Basseville, 1988, Patton et al., 2000].

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Model-based FDI Techniques (Cont'd)

➤ Modelling of Faulty Systems

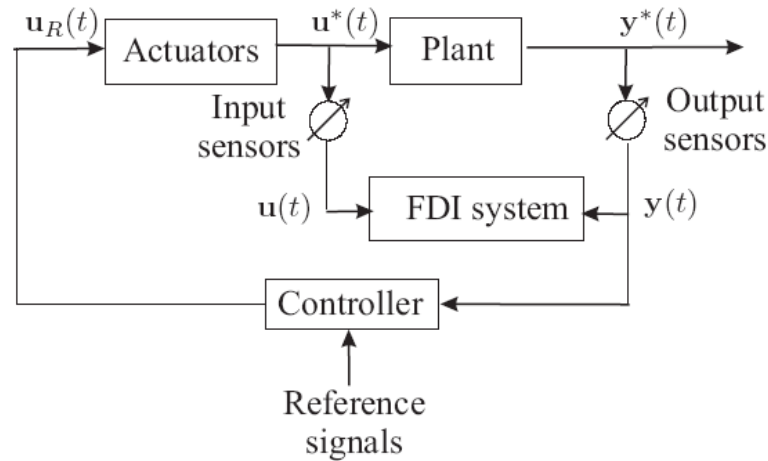


Figure 2.2: Fault diagnosis in a closed-loop system.

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Model-based FDI Techniques (Cont'd)

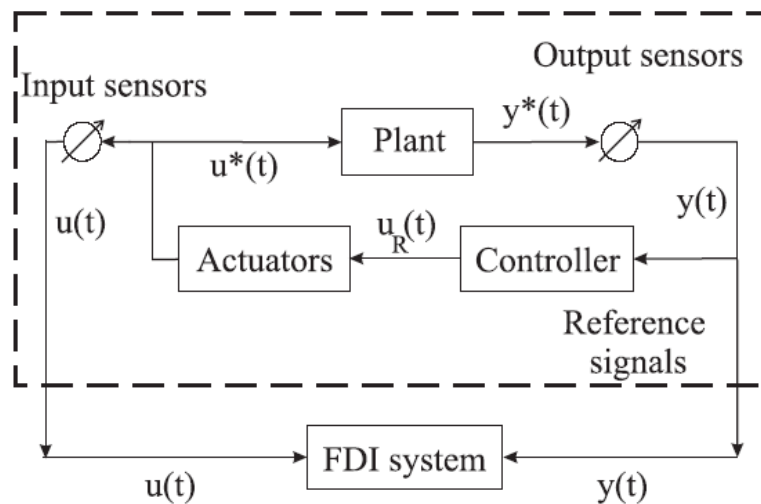


Figure 2.3: The rearranged fault diagnosis scheme.

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Model-based FDI Techniques (Cont'd)

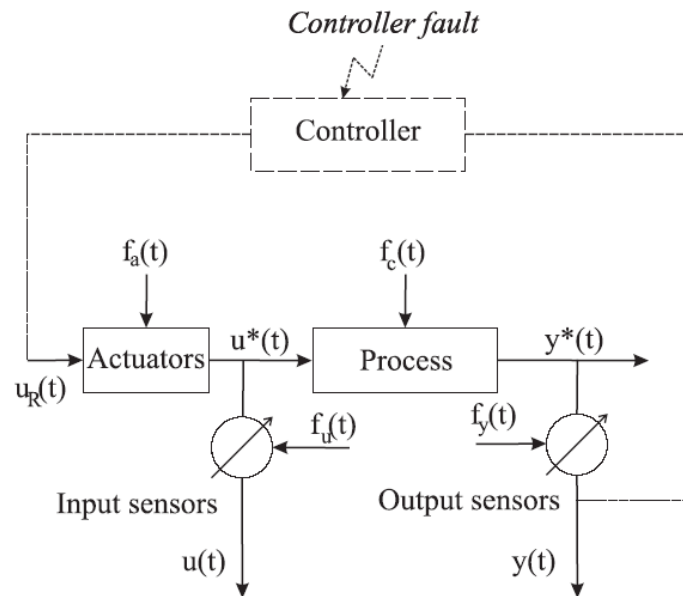


Figure 2.4: The controlled system and fault topology.

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Model-based FDI Techniques (Cont'd)

Fault Location:

- Actuators
- Process or system components
- Input sensors
- Output sensors
- Controllers

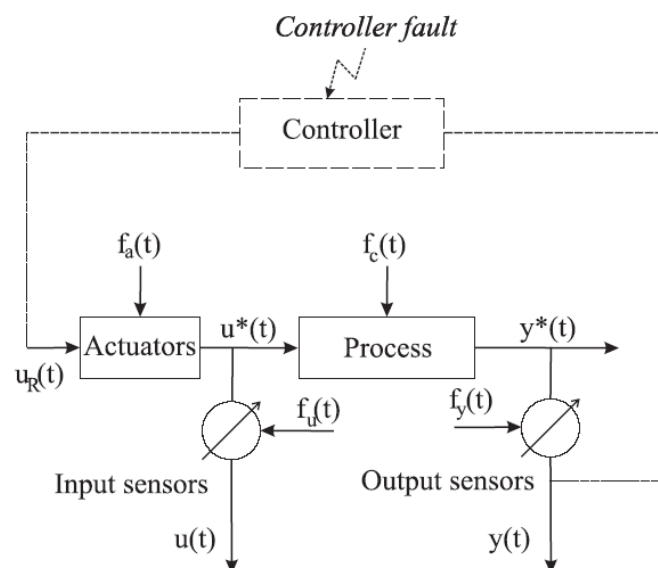


Figure 2.4: The controlled system and fault topology.

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Model-based FDI Techniques (Cont'd)

Fault and System Modelling

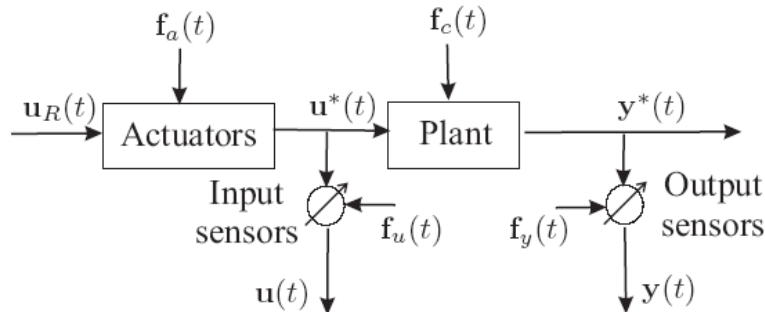


Figure 2.5: The monitored system and fault topology.

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}^*(t) \\ \mathbf{y}^*(t) &= \mathbf{C}\mathbf{x}(t) \end{cases}$$

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Model-based FDI Techniques (Cont'd)

Fault and System Modelling

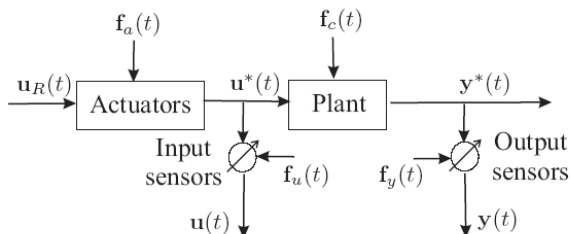


Figure 2.5: The monitored system and fault topology.

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}^*(t) \\ \mathbf{y}^*(t) &= \mathbf{C}\mathbf{x}(t) \end{cases}$$

$$\mathbf{x}(t+1) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}^*(t) + \mathbf{f}_c(t)$$

$$\mathbf{f}_c(t) = \mathbf{I}_i \Delta a_{ij} x_j(t)$$

$$\begin{cases} \mathbf{u}(t) &= \mathbf{u}^*(t) + \mathbf{f}_u(t) \\ \mathbf{y}(t) &= \mathbf{y}^*(t) + \mathbf{f}_y(t) \end{cases}$$

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Model-based FDI Techniques (Cont'd)

Fault and System Modelling

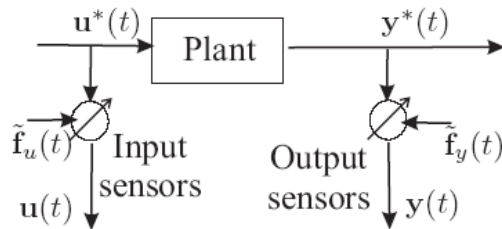


Figure 2.6: The structure of the plant sensors.

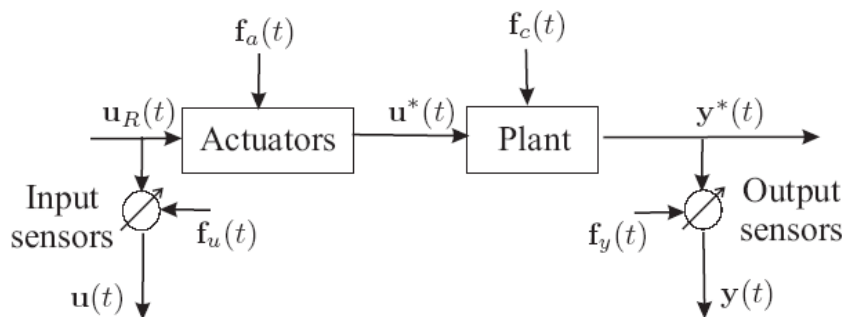
$$\begin{cases} \mathbf{u}(t) = \mathbf{u}^*(t) + \tilde{\mathbf{u}}(t) \\ \mathbf{y}(t) = \mathbf{y}^*(t) + \tilde{\mathbf{y}}(t) \end{cases}$$

$$\begin{cases} \mathbf{u}(t) = \mathbf{u}^*(t) + \tilde{\mathbf{u}}(t) + \mathbf{f}_u(t) \\ \mathbf{y}(t) = \mathbf{y}^*(t) + \tilde{\mathbf{y}}(t) + \mathbf{f}_y(t) \end{cases}$$

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Model-based FDI Techniques (Cont'd)

Fault and System Modelling

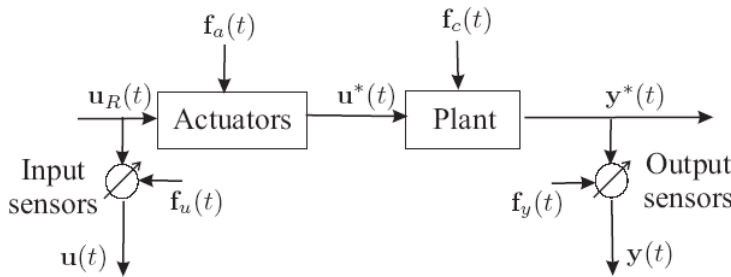


$$\mathbf{u}^*(t) = \mathbf{u}_R(t) + \mathbf{f}_a(t)$$

$$\begin{cases} \mathbf{x}(t+1) = \mathbf{A} \mathbf{x}(t) + \mathbf{f}_c(t) + \mathbf{B} \mathbf{u}_R(t) \\ \mathbf{y}(t) = \mathbf{C} \mathbf{x}(t) + \mathbf{f}_y(t) \\ \mathbf{u}(t) = \mathbf{u}_R(t) + \mathbf{f}_u(t) \end{cases}$$

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Model-based FDI Techniques (Cont'd)

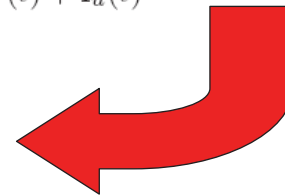


Modelling of Faulty Systems

Figure 2.7: Fault topology with actuator input signal measurement.

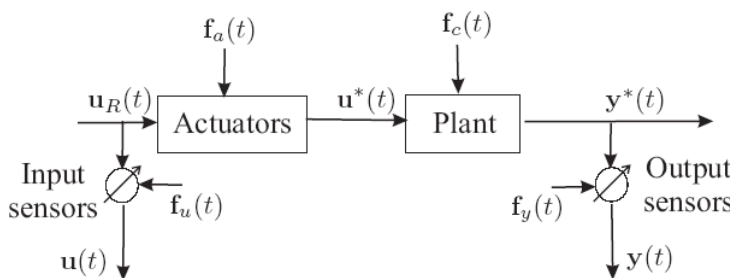
$$\mathbf{f}(t) = [\mathbf{f}_a^T, \mathbf{f}_u^T, \mathbf{f}_c^T, \mathbf{f}_y^T]^T \in \mathbb{R}^k \quad \begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{f}_c(t) + \mathbf{B}\mathbf{f}_a(t) + \mathbf{B}\mathbf{u}^*(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{f}_y(t) \\ \mathbf{u}(t) &= \mathbf{u}^*(t) + \mathbf{f}_u(t) \end{cases}$$

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}^*(t) + \mathbf{L}_1\mathbf{f}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{L}_2\mathbf{f}(t) \\ \mathbf{u}(t) &= \mathbf{u}^*(t) + \mathbf{L}_3\mathbf{f}(t) \end{cases}$$



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Model-based FDI Techniques (Cont'd)



Modelling of Faulty Systems

Figure 2.7: Fault topology with actuator input signal measurement.

$$\mathbf{y}(z) = \mathbf{G}_{yu^*}(z)\mathbf{u}^*(z) + \mathbf{G}_{yf}(z)\mathbf{f}(z)$$

Transfer function description:

$$\begin{cases} \mathbf{G}_{yu^*}(z) &= \mathbf{C}(z\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} \\ \mathbf{G}_{yf}(z) &= \mathbf{C}(z\mathbf{I} - \mathbf{A})^{-1}\mathbf{L}_1 + \mathbf{L}_2 \end{cases}$$

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Residual Generator Structure

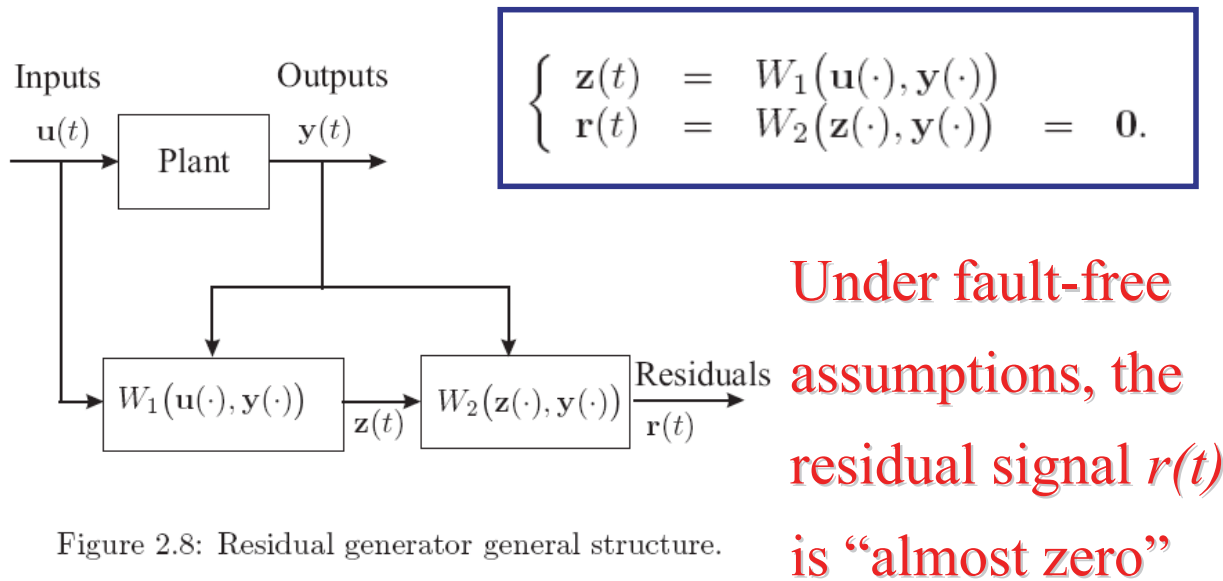


Figure 2.8: Residual generator general structure.

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Residual General Structure (Cont'd)

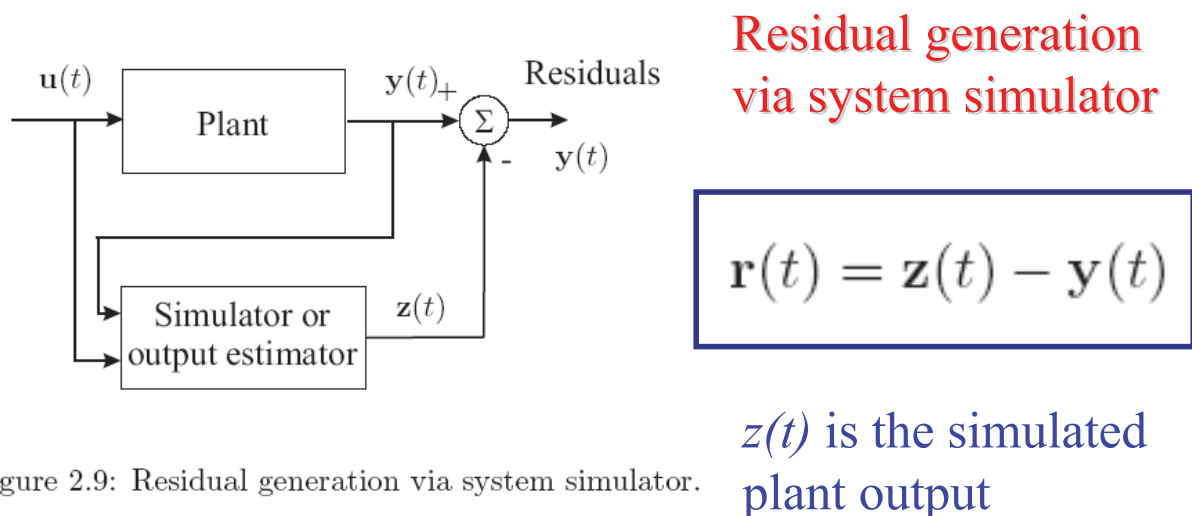
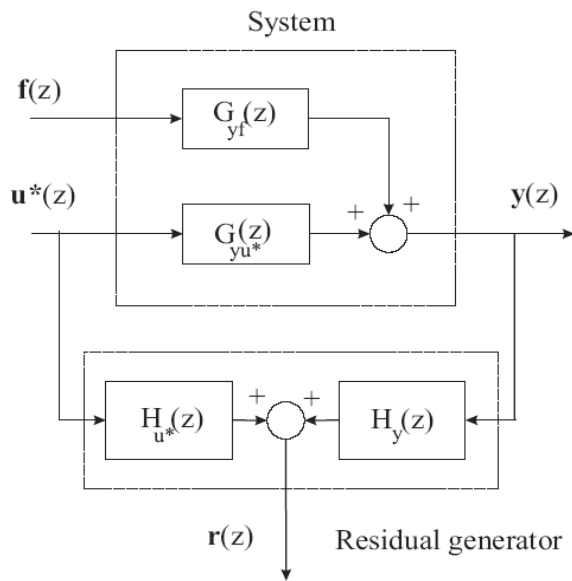


Figure 2.9: Residual generation via system simulator.

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Residual General Structure (Cont'd)



$$y(z) = G_{yu^*}(z)u^*(z) + G_{yf}(z)f(z)$$

Residual generator:

$$r(z) = \begin{bmatrix} H_{u^*}(z) & H_y(z) \end{bmatrix} \begin{bmatrix} u^*(z) \\ y(z) \end{bmatrix} =$$

$$= H_{u^*}(z)u^*(z) + H_y(z)y(z)$$

$$r(t) = 0 \text{ if and only if } f(t) = 0$$

Constraint conditions: design

$$H_{u^*}(z) + H_y(z)G_{yu^*} = 0$$

Figure 2.10: Residual generator general structure.
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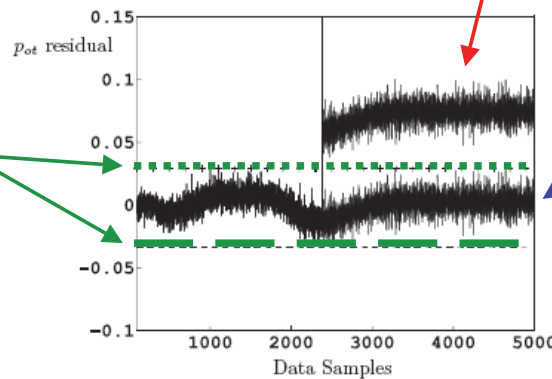
General Residual Evaluation

$$\begin{cases} J(r(t)) \leq \varepsilon(t) & \text{for } f(t) = 0 \\ J(r(t)) > \varepsilon(t) & \text{for } f(t) \neq 0 \end{cases}$$

Detection thresholds $\varepsilon(t)$

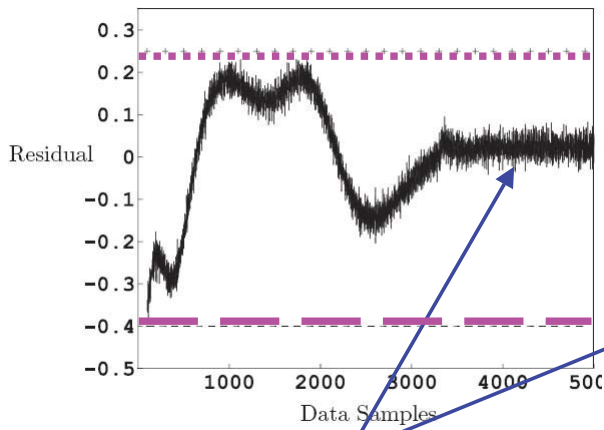
Faulty residual

Fault free residual

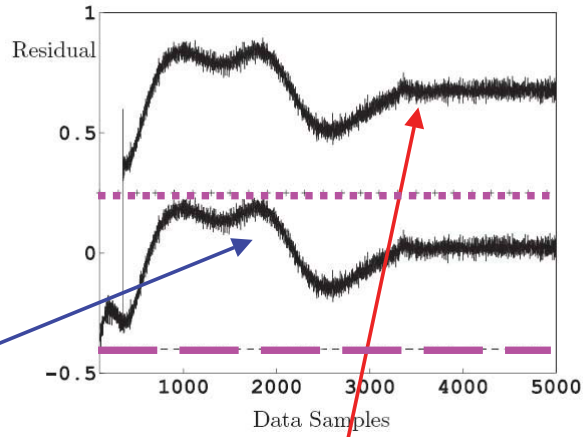


General Residual Evaluation *(example)*

Detection thresholds



Fault free residual



Fault-free & faulty residuals

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Residual Generation Techniques

- Fault detection via parameter estimation
- Observer-based approaches
- Parity (vector) relations

15/04/2011



Fault Detection via Parameter Estimation

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Parameter Estimation

- Parameter estimation for fault detection
- The process parameters are not known at all, or they are not known exactly enough. They can be determined with parameter estimation methods
- The basic structure of the model has to be known
- Based on the assumption that the faults are reflected in the physical system parameters
- The parameters of the actual process are estimated on-line using well-known parameter estimations methods

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Parameter Estimation (Cont'd)

- The results are thus compared with the parameters of the reference model obtained initially under fault-free assumptions
- Any discrepancy can indicate that a fault may have occurred
- **An approach for modelling the input-output behaviour of the monitored system will be recalled and exploited for fault detection**

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Equation Error Approach

- SISO model

$$y(t) = \Psi^T \Theta$$

- Parameter vector

$$\Theta^T = [a_1 \dots a_n, b_1 \dots b_n]$$

- Regression vector

$$\Psi^T = [y(t-1) \dots y(t-n) \quad u(t-1) \dots u(t-n)]$$

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Equation Error Method

- Equation error

$$e(t) = y(t) - \Psi^T \Theta$$

- Model of the process (Z-transform)

$$\frac{y(z)}{u(z)} = \frac{B(z)}{A(z)}$$

- Estimated polynomials

$$e(t) = \hat{B}(z)u(t) - \hat{A}(z)y(t)$$

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Equation Error Method (Cont'd)

- Estimation of the process model: LS

$$\hat{\Theta} = [\Psi^T \Psi]^{-1} \Psi^T y$$

- LS minimisation

$$\begin{cases} J(\Theta) & = \sum_t e^2(t) = e^T e \\ \frac{d J(\Theta)}{d \Theta} & = \mathbf{0}. \end{cases}$$

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Equation Error Method (Cont'd)

- Estimation of the process model: **RLS**

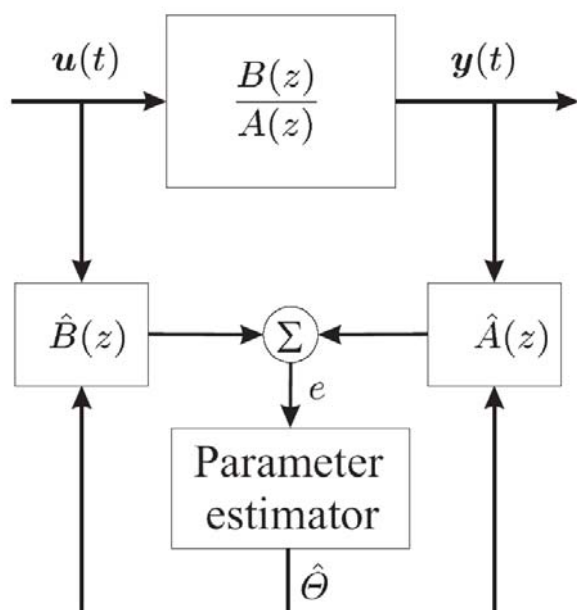
$$\hat{\Theta}(t+1) = \hat{\Theta}(t) + \gamma(t) \left[y(t) - \Psi^T(t) \hat{\Theta}(t) \right]$$

- Estimate recursive adaptation

$$\begin{cases} \gamma(t) &= \frac{1}{\Psi^T(t+1) \mathbf{P}(t) \Psi(t+1) + 1} \mathbf{P}(t) \Psi(t+1) \\ \mathbf{P}(t+1) &= [I - \gamma(t) \Psi^T(t+1)] \mathbf{P}(t). \end{cases}$$

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Parameter Estimation via EE



- Recursive estimation of the transfer function polynomials
- Equation error
- Parameter estimation via recursive algorithm
- **RLS**

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Links Between Input-Output and State-Space Discrete-Time LTI Models

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Input-Output Model (EE)

- The input to output discrete-time model behaviour can be mathematically described by a set of ARX Multi-Input Single-Output (MISO) models

$$y_i^*(t) = \sum_{j=1}^n \alpha_{i,j} y_i^*(t-j) + \sum_{j=1}^r \sum_{k=1}^n \beta_{i,j,k} u_j^*(t-k) + \varepsilon_i(t), \quad i = 1, \dots, m$$

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Input-Output Model (EE)

- m is the number of the output variables. The order n and the parameters $\alpha_{i,j}$ and $\beta_{i,j,k}$ with $i = 1, \dots, m$, of the model are determined by the identification approach. The term $\varepsilon_i(t)$ takes into account the modelling error (EE)

$$y_i^*(t) = \sum_{j=1}^n \alpha_{i,j} y_i^*(t-j) + \sum_{j=1}^r \sum_{k=1}^n \beta_{i,j,k} u_j^*(t-k) + \varepsilon_i(t), \quad i = 1, \dots, m$$

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State-Space Equivalent Model

- The input-output EE model has a state space "realisation" as follows:

$$\begin{cases} \mathbf{x}_i(t+1) &= \mathbf{A}_i \mathbf{x}_i(t) + \mathbf{B}_i \mathbf{u}^*(t) + \mathbf{B}_{\omega_i} \varepsilon_i & i = 1, \dots, m \\ \mathbf{y}_i^*(t) &= \mathbf{C}_i \mathbf{x}_i(t) + \mathbf{D}_{\omega_i} \varepsilon_i, & t = 1, 2, \dots \end{cases}$$

- The matrices $(\mathbf{A}_i, \mathbf{B}_i, \mathbf{C}_i, \mathbf{B}_{\omega_i}, \mathbf{D}_{\omega_i})$ of a state space representation in canonical form of the n -th order system are defined as follows:

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State-Space Matrices

$$A_i = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \alpha_{i,1} & \alpha_{i,2} & \alpha_{i,3} & \cdots & \alpha_{i,n} \end{bmatrix},$$

$$C_i = [1 \ 0 \ \cdots \ 0],$$

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State-Space Matrices (Cont'd)

$$\begin{bmatrix} B_i & B_{\omega_i} \\ 0 & D_{\omega_i} \end{bmatrix} = S_i^{-1} \begin{bmatrix} \beta_{i,1,1} & \cdots & \beta_{i,r,1} & 0 \\ \vdots & \vdots & \vdots & \vdots \\ \beta_{i,1,n} & \cdots & \beta_{i,r,n} & 0 \\ 0 & \cdots & 0 & 1 \end{bmatrix}$$

$$S_i = \begin{bmatrix} -\alpha_{i,1} & -\alpha_{i,2} & \cdots & -\alpha_{i,n} & 1 \\ -\alpha_{i,2} & -\alpha_{i,3} & \cdots & 1 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -\alpha_{i,n} & 1 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \end{bmatrix}$$

Note that the matrix S_i is always non-singular

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State-Space Matrices (Cont'd)

TF2SS Transfer function to state-space conversion

[A,B,C,D] = TF2SS(NUM,DEN) calculates the state-space representation (A,B,C,D) of the system (NUM,DEN) from a single input. Vector **DEN** must contain the coefficients of the denominator in descending powers of s (z). Matrix **NUM** must contain the numerator coefficients with as many rows as there are outputs y . The A,B,C,D matrices are returned in controller canonical form. This calculation also works for discrete systems

For **MIMO** models, use **ss** and **tf** Matlab functions

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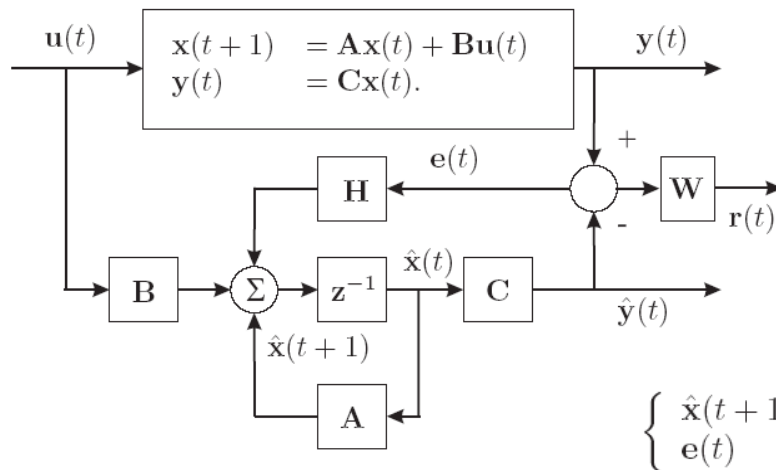


Observer-based Approaches

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Residual General Structure

Observer-based approach



Plant model

$$\begin{cases} x(t+1) = Ax(t) + Bu(t) \\ y(t) = Cx(t) \end{cases}$$

Observer model

$$\begin{cases} \hat{x}(t+1) = A\hat{x}(t) + Bu(t) + He(t) \\ e(t) = y(t) - C\hat{x}(t) \end{cases}$$

Output estimation approach!

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Residual Generator Structure

Plant model

$$\begin{cases} x(t+1) = Ax(t) + Bu(t) \\ y(t) = Cx(t) \end{cases}$$

Observer model

$$\begin{cases} \hat{x}(t+1) = A\hat{x}(t) + Bu(t) + He(t) \\ e(t) = y(t) - C\hat{x}(t) \end{cases}$$

State estimation model

$$\begin{cases} e_x(t) = x(t) - \hat{x}(t) \\ e_x(t+1) = (A - HC)e_x(t) \end{cases}$$

State estimation property

$$\lim_{t \rightarrow \infty} e_x(t) = 0 \quad (\text{fault-free case!!!})$$

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Residual Generator Property

+ disturbance signals and fault

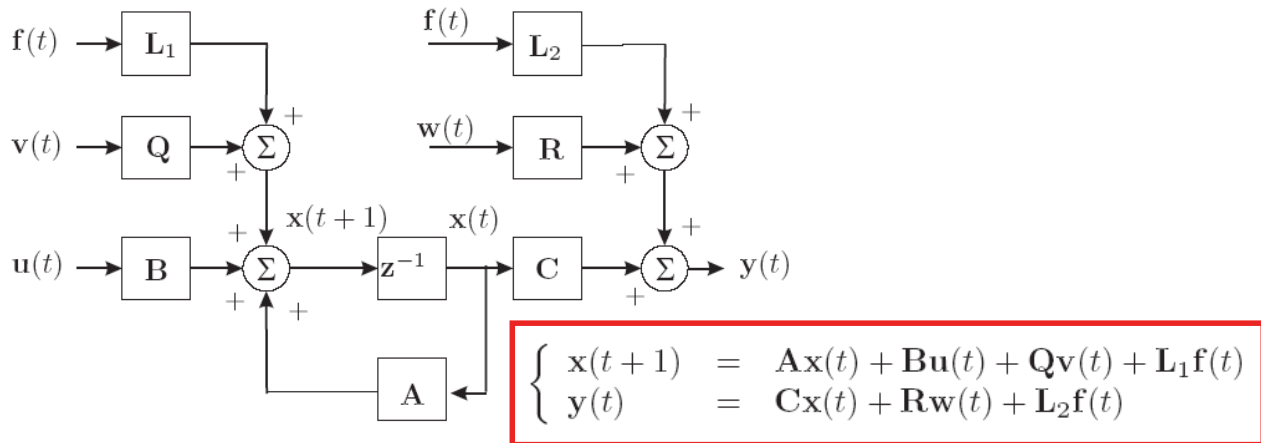


Figure 2.14: MIMO process with faults and noises.

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Residual Generator Property (Cont'd)

+ fault signals

System model

$$\begin{cases} x(t+1) = Ax(t) + Bu(t) + Qv(t) + L_1f(t) \\ y(t) = Cx(t) + Rw(t) + L_2f(t) \end{cases}$$

Observer model

$$e_x(t+1) = (A - HC)e_x(t) + L_1f(t) - HL_2f(t)$$

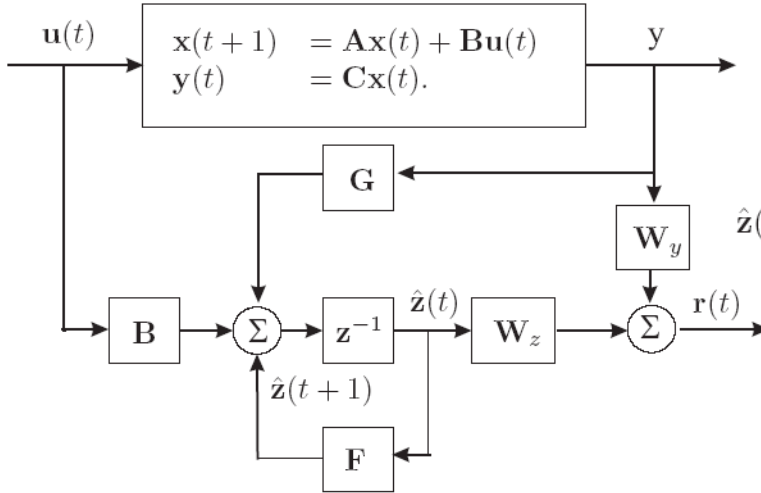
Output estimation error with faults but noise-free

$$e(t) = Ce_x(t) + L_2f(t).$$

Both $e(t)$ and $e_x(t)$ are suitable residuals!

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Output Observer & UIO: *intro*



State transformation

$$z(t) = \mathbf{T}x(t)$$

Observer

$$\hat{z}(t+1) = \mathbf{F}\hat{z}(t) + \mathbf{J}u(t) + \mathbf{G}y(t)$$

Residual

$$r(t) = \mathbf{W}_z \hat{z}(t) + \mathbf{W}_y y(t)$$

State estimation error

$$e_x(t) = \hat{z}(t) - z(t) = \hat{z}(t) - \mathbf{T}x(t)$$

Figure 2.15: Process and output observer.

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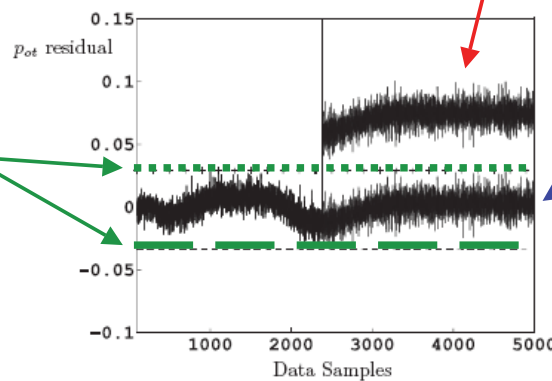
General Residual Evaluation

$$\begin{cases} J(\mathbf{r}(t)) \leq \varepsilon(t) & \text{for } \mathbf{f}(t) = \mathbf{0} \\ J(\mathbf{r}(t)) > \varepsilon(t) & \text{for } \mathbf{f}(t) \neq \mathbf{0} \end{cases}$$

Detection thresholds $\varepsilon(t)$

Faulty residual

Fault free residual



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Change Detection & Residual Evaluation

$$\begin{cases} J(\mathbf{r}(t)) \leq \varepsilon(t) & \text{for } \mathbf{f}(t) = \mathbf{0} \\ J(\mathbf{r}(t)) > \varepsilon(t) & \text{for } \mathbf{f}(t) \neq \mathbf{0} \end{cases}$$

$$J(\mathbf{r}(t)) \equiv |\mathbf{r}(t)|$$

Detection thresholds

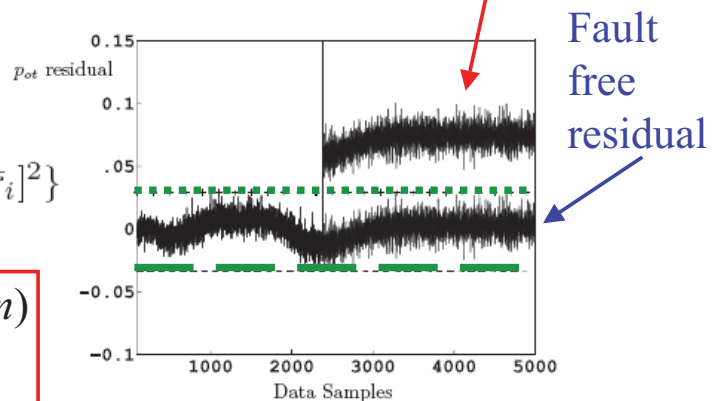
$$\varepsilon(t)$$

$$\bar{r}_i = E\{r_i(t)\}; \quad \bar{\sigma}_i^2 = E\{[r_i(t) - \bar{r}_i]^2\}$$

$$\varepsilon(t) = \bar{r}_i \pm \delta \times \bar{\sigma}_i \quad (i = 1, \dots, m)$$

with $\delta \geq 3$

Faulty residual



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Residual Generation

✓ Output Observers

➤ Unknown Input Observers

✓ Fault Detection

➤ Fault Isolation, *i.e. where is the fault?*

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Output Observer

Process model with faults

$$\begin{aligned} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}(\mathbf{u}(t) + \mathbf{f}_c(t)) + \mathbf{f}_s(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t), \end{aligned}$$

Input-output sensor faults

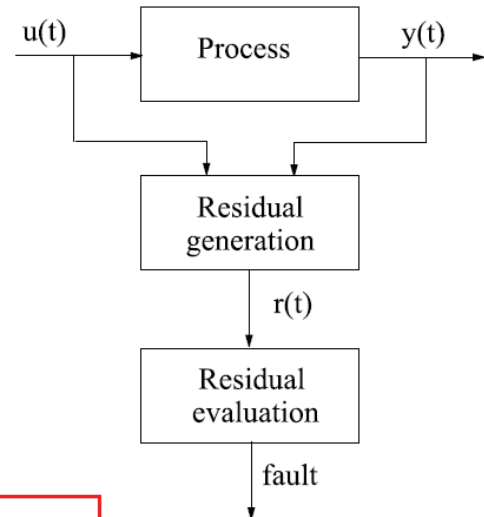
$$\left. \begin{aligned} \mathbf{u}(t) &= \mathbf{f}_u(t) + \mathbf{u}^*(t) \\ \mathbf{y}(t) &= \mathbf{f}_y(t) + \mathbf{y}^*(t) \end{aligned} \right\}$$

Observer for the i -th output $y_i(t)$

$$\mathbf{x}^i(t+1) = \mathbf{A}_i \mathbf{x}^i(t) + \mathbf{B}_i \mathbf{u}(t) + \mathbf{K}_i (y_i(t) - \mathbf{C}_i \mathbf{x}^i(t))$$

$(\mathbf{A}_i, \mathbf{B}_i, \mathbf{C}_i)$ is the state-space process model

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Output Observer for *Fault Detection*

Given the observer model

$$\mathbf{x}^i(t+1) = \mathbf{A}_i \mathbf{x}^i(t) + \mathbf{B}_i \mathbf{u}(t) + \mathbf{K}_i (y_i(t) - \mathbf{C}_i \mathbf{x}^i(t))$$

Under fault-free assumptions

$$r_i(t) = y_i^*(t) - \hat{y}_i(t) = \mathbf{C}_i (\mathbf{x}_i(t) - \mathbf{x}^i(t)) \text{ is equal to zero.}$$

Fault detection logic

fixed threshold ϵ ,

$$\left. \begin{aligned} r(t) &\leq \epsilon && \text{for } \mathbf{f}(t) = \mathbf{0} \\ r(t) &> \epsilon && \text{for } \mathbf{f}(t) \neq \mathbf{0} \end{aligned} \right\}$$

$\mathbf{f}(t)$ being a generic failure vector.

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Output Observer for *Fault Isolation*

$$\left. \begin{aligned} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{B}\mathbf{f}_u(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{f}_y(t) \end{aligned} \right\}$$

Process model

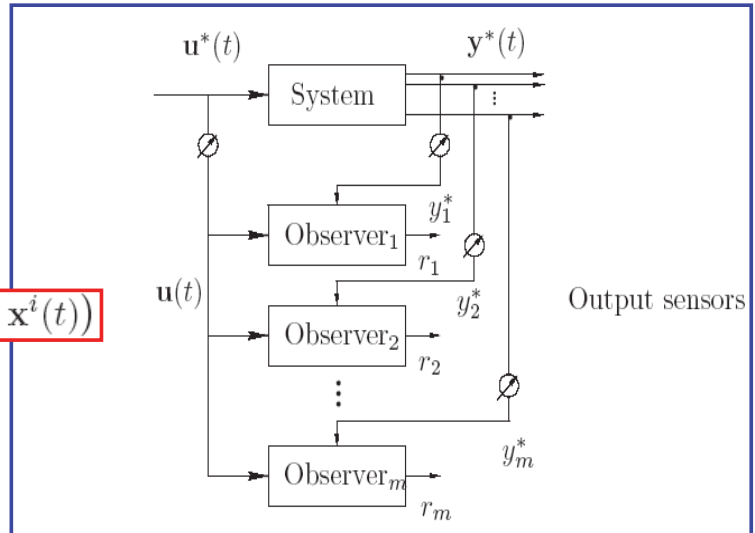
$$\mathbf{x}^i(t+1) = \mathbf{A}_i\mathbf{x}^i(t) + \mathbf{B}_i\mathbf{u}(t) + \mathbf{K}_i(y_i(t) - \mathbf{C}_i\mathbf{x}^i(t))$$

$$r_i(t) = y_i^*(t) - \hat{y}_i(t) = \mathbf{C}_i(\mathbf{x}_i(t) - \mathbf{x}^i(t))$$

$$y_i(t) = y_i^*(t) + f(t)$$

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Bank of output observers



Output Observer for *Fault Isolation* (Cont'd)

$$\mathbf{x}^i(t+1) = \mathbf{A}_i\mathbf{x}^i(t) + \mathbf{B}_i\mathbf{u}(t) + \mathbf{K}_i(y_i(t) - \mathbf{C}_i\mathbf{x}^i(t))$$

$$r_i(t) = y_i^*(t) - \hat{y}_i(t) = \mathbf{C}_i(\mathbf{x}_i(t) - \mathbf{x}^i(t))$$

Fault-free case:

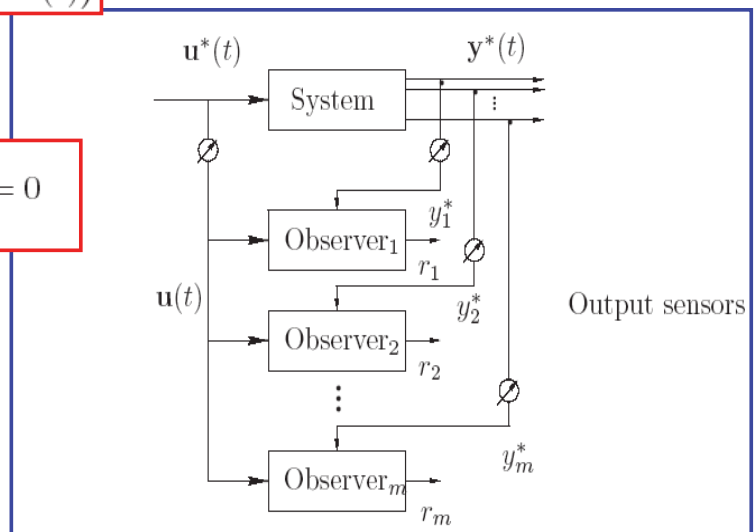
$$\lim_{t \rightarrow \infty} r_i(t) = \lim_{t \rightarrow \infty} (y_i(t) - \mathbf{C}_i\mathbf{x}^i(t)) = 0$$

Faulty case

$$y_i(t) = y_i^*(t) + f(t)$$

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Bank of output observers



Output Observer for *Fault Isolation* (Cont'd)

Table 4.1: Fault signatures.

	u_1	u_2	...	u_r	y_1	y_2	...	y_m
r_{O_1}	1	1	...	1	1	0	...	0
r_{O_2}	1	1	...	1	0	1	...	0
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots
r_{O_m}	1	1	...	1	0	0	...	1

$$\mathbf{x}^i(t+1) = \mathbf{A}_i \mathbf{x}^i(t) + \mathbf{B}_i \mathbf{u}(t) + \mathbf{K}_i (y_i(t) - \mathbf{C}_i \mathbf{x}^i(t))$$

Fault-free case:

$$\lim_{t \rightarrow \infty} r_i(t) = \lim_{t \rightarrow \infty} (y_i(t) - \mathbf{C}_i \mathbf{x}^i(t)) = 0$$

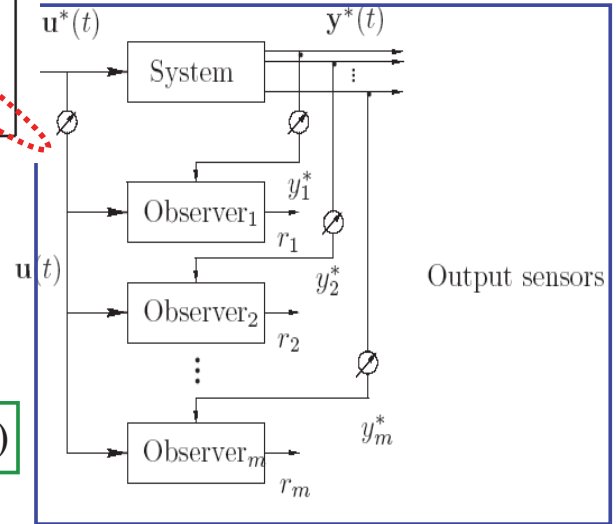
Faulty case

$$y_i(t) = y_i^*(t) + f(t)$$

$$\lim_{t \rightarrow \infty} r_i(t) \neq 0$$

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Bank of output observers



Unknow Input Observer (UIO)

$$\left. \begin{aligned} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{E}\mathbf{d}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) \end{aligned} \right\} \begin{array}{l} \text{Disturbance Distribution Matrix (Known)} \\ \text{System with disturbance} \\ \text{"Unknown Input"} \end{array}$$

↑
Unknown Input

Definition: An observer is defined as an *Unknown Input Observer* for the system with disturbance (above), if its state estimation error vector $e_x(t)$ approaches zero asymptotically, regardless of the presence of the unknown input term in the system.

UIO Model

Given:

$$\left. \begin{aligned} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{E}\mathbf{d}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) \end{aligned} \right\}$$

The full-order UIO has the following mathematical form

$$\left. \begin{aligned} \mathbf{z}(t+1) &= \mathbf{F}\mathbf{z}(t) + \mathbf{T}\mathbf{B}\mathbf{u}(t) + \mathbf{K}\mathbf{y}(t) \\ \hat{\mathbf{x}}(t) &= \mathbf{z}(t) + \mathbf{H}\mathbf{y}(t) \end{aligned} \right\}$$

where $\mathbf{z}(t) \in \mathbb{R}^n$ is the state of the UIO, $\hat{\mathbf{x}}(t)$ the estimated state vector $\mathbf{x}(t)$, whilst \mathbf{F} , \mathbf{T} , \mathbf{H} and \mathbf{K} are matrices to be designed to achieve the unknown input de-coupling .

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UIO Structure

Plant Model

$$\left. \begin{aligned} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{E}\mathbf{d}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) \end{aligned} \right\}$$

UIO Model

$$\left. \begin{aligned} \mathbf{z}(t+1) &= \mathbf{F}\mathbf{z}(t) + \mathbf{T}\mathbf{B}\mathbf{u}(t) + \mathbf{K}\mathbf{y}(t) \\ \hat{\mathbf{x}}(t) &= \mathbf{z}(t) + \mathbf{H}\mathbf{y}(t) \end{aligned} \right\}$$

Observer Design???

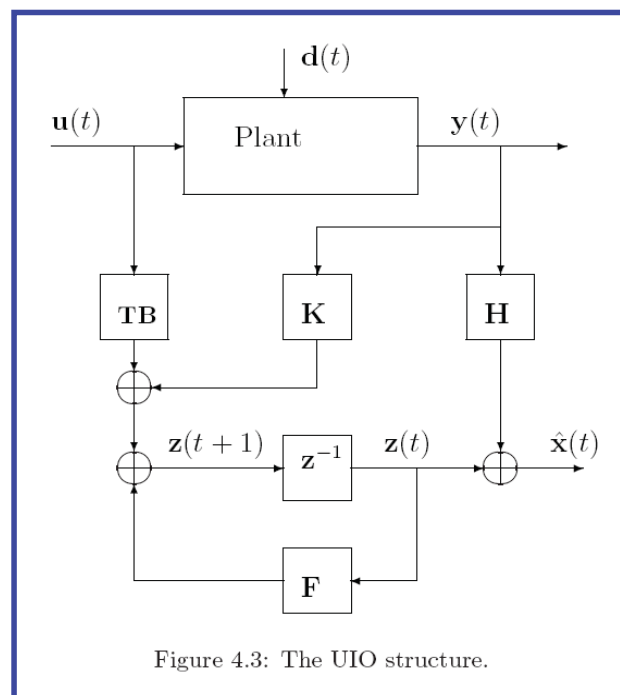


Figure 4.3: The UIO structure.

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UIO Design

$$\left. \begin{aligned} x(t+1) &= \mathbf{A}x(t) + \mathbf{B}u(t) + \mathbf{E}d(t) \\ y(t) &= \mathbf{C}x(t) \end{aligned} \right\} \text{Plant Model}$$

$$\left. \begin{aligned} z(t+1) &= \mathbf{F}z(t) + \mathbf{T}Bu(t) + \mathbf{K}y(t) \\ \hat{x}(t) &= z(t) + \mathbf{H}y(t) \end{aligned} \right\} \text{UIO Model}$$

$$e_x(t+1) = x(t+1) - \hat{x}(t+1) \quad \text{State estimation error}$$

$$\begin{aligned} e_x(t+1) &= [\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C}]e_x(t) + [\mathbf{F} - (\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C})]z(t) \\ &+ [\mathbf{K}_2 - (\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C})]y(t) \\ &+ [\mathbf{T} - (\mathbf{I} - \mathbf{HC})]\mathbf{B}u(t) + (\mathbf{HC} - \mathbf{I})\mathbf{E}d(t) \end{aligned}$$

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UIO Design (Cont'd)

$$\begin{aligned} e_x(t+1) &= [\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C}]e_x(t) + [\mathbf{F} - (\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C})]z(t) \\ &+ [\mathbf{K}_2 - (\mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C})]y(t) \\ &+ [\mathbf{T} - (\mathbf{I} - \mathbf{HC})]\mathbf{B}u(t) + (\mathbf{HC} - \mathbf{I})\mathbf{E}d(t) \end{aligned}$$

$$\left. \begin{aligned} z(t+1) &= \mathbf{F}z(t) + \mathbf{T}Bu(t) + \mathbf{K}y(t) \\ \hat{x}(t) &= z(t) + \mathbf{H}y(t) \end{aligned} \right\}$$

$$\begin{aligned} (\mathbf{HC} - \mathbf{I})\mathbf{E} &= \mathbf{0} \\ \mathbf{I} - \mathbf{HC} &= \mathbf{T} \\ \mathbf{A} - \mathbf{HCA} - \mathbf{K}_1\mathbf{C} &= \mathbf{F} \\ \mathbf{FH} &= \mathbf{K}_2 \end{aligned}$$

the state estimation error will then be:

$$e_x(t+1) = \mathbf{F}e_x(t).$$

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UIO Design (Cont'd)

$$\left. \begin{aligned} x(t+1) &= Ax(t) + Bu(t) + Ed(t) \\ y(t) &= Cx(t) \end{aligned} \right\}$$

$$\left. \begin{aligned} z(t+1) &= Fz(t) + TBu(t) + Ky(t) \\ \hat{x}(t) &= z(t) + Hy(t) \end{aligned} \right\}$$

$$\begin{aligned} (HC - I)E &= 0 \\ I - HC &= T \\ A - HCA - K_1C &= F \\ FH &= K_2 \end{aligned}$$

$$e_x(t+1) = Fe_x(t).$$

This means that, if all the eigenvalues of F are stable, $e_x(t)$ will approach zero asymptotically, *i.e.*, $\hat{x}(t) \rightarrow x(t)$. Hence, according to the definition of the UIO described by the model above, it is an UIO for the monitored system. The design of this UIO consists of solving the equation system and making all eigenvalues of the system matrix F be stable.

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UIO Design (Cont'd)

$$\left. \begin{aligned} x(t+1) &= Ax(t) + Bu(t) + Ed(t) \\ y(t) &= Cx(t) \end{aligned} \right\} \quad **$$

$$\left. \begin{aligned} z(t+1) &= Fz(t) + TBu(t) + Ky(t) \\ \hat{x}(t) &= z(t) + Hy(t) \end{aligned} \right\} \quad *$$

$$\begin{aligned} (HC - I)E &= 0 \quad *** \\ I - HC &= T \\ A - HCA - K_1C &= F \\ FH &= K_2 \end{aligned}$$

Theorem Necessary and sufficient conditions for the existence of an UIO
* for the system defined by Equation ** are [Chen & Patton, 1999]:

1. $\text{rank}(CE) = \text{rank}(E)$,
2. (A_1, C) is a detectable pair,

where $A_1 = A - E(CE)^+CA$.

A special solution for the matrix H in conditions *** is given by [Chen & Patton, 1999]:

$$H^* = E(CE)^+$$

where $(\cdot)^+$ is the pseudoinverse of the matrix CE .

15/04/2011

UIO for Fault (Detection) + Isolation

$$\left. \begin{aligned} x(t+1) &= Ax(t) + Bu(t) + Ed(t) \\ y(t) &= Cx(t) \end{aligned} \right\}$$

General system

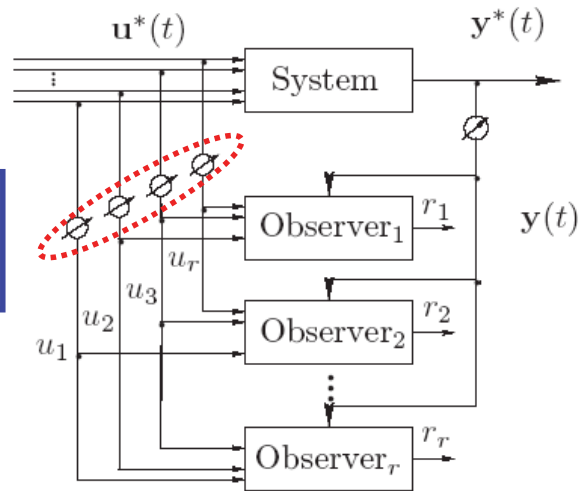
$$\left. \begin{aligned} z(t+1) &= Fz(t) + TBu(t) + Ky(t) \\ \hat{x}(t) &= z(t) + Hy(t) \end{aligned} \right\}$$

UIO model

$$\left. \begin{aligned} x(t+1) &= Ax(t) + Bu(t) + Bf_u(t) \\ y(t) &= Cx(t) + f_y(t) \end{aligned} \right\}$$

Process with input faults

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Input sensors

Output sensors are fault-free

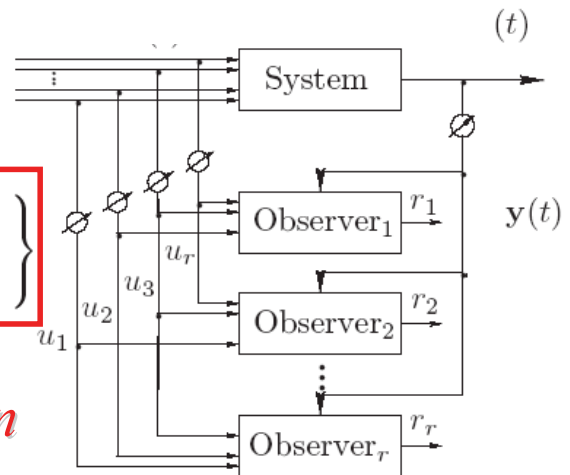
UIO for FDI

With reference to the devices for the FDI of the inputs, depicted in Figure 4.5, the structure of the i -th UIO ($i = 1, 2, \dots, r$) for residual generation [Chen & Patton, 1999], under the assumptions $\tilde{u}(t) \cong 0$, $\tilde{y}(t) \cong 0$ and $f_y(t) = 0$, is the following

$$\left. \begin{aligned} z^i(t+1) &= (T^i A - K^i C)z^i(t) + J^i u(t) + S^i y(t) \\ r^i(t) &= L_1^i z^i(t) + L_2^i y(t) \end{aligned} \right\}$$

UIO for Residual Generation

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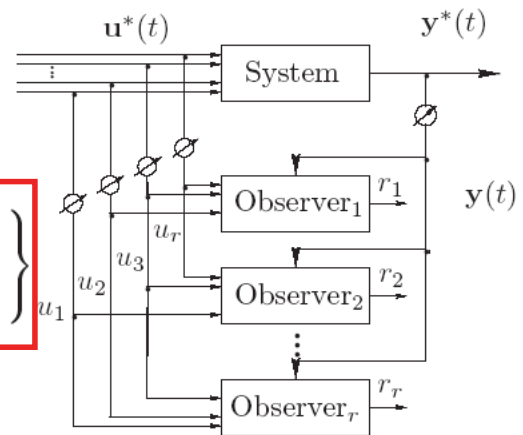


Input sensors

UIO for FDI (Cont'd)

UIO for Residual Generation

$$\left. \begin{aligned} \mathbf{z}^i(t+1) &= (\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}) \mathbf{z}^i(t) + \mathbf{J}^i \mathbf{u}(t) + \mathbf{S}^i \mathbf{y}(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{z}^i(t) + \mathbf{L}_2^i \mathbf{y}(t) \end{aligned} \right\} u_1$$



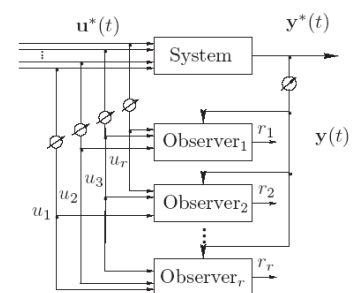
Input sensors

where $\mathbf{z}^i(t) \in \mathbb{R}^n$ denotes the observer state vector, $\mathbf{r}^i(t) \in \mathbb{R}^m$ is the residual vector and \mathbf{F}^i , \mathbf{J}^i , \mathbf{S}^i , \mathbf{L}_1^i and \mathbf{L}_2^i are matrices to be designed with appropriate dimensions. Let \mathbf{T}^i be a linear transformation of the state $\mathbf{x}(t)$ of the system and define the state estimation error as $\mathbf{e}_x^i(t) = \mathbf{z}^i(t) - \mathbf{T}^i \mathbf{x}(t)$.

15/04/2011

UIO for FDI (Cont'd)

$$\left. \begin{aligned} \mathbf{z}^i(t+1) &= (\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}) \mathbf{z}^i(t) + \mathbf{J}^i \mathbf{u}(t) + \mathbf{S}^i \mathbf{y}(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{z}^i(t) + \mathbf{L}_2^i \mathbf{y}(t) \end{aligned} \right\}$$



Input sensors

define the state estimation error as $\mathbf{e}_x^i(t) = \mathbf{z}^i(t) - \mathbf{T}^i \mathbf{x}(t)$. On the suppositions $\tilde{\mathbf{u}}(t) = \mathbf{0}$, $\tilde{\mathbf{y}}(t) = \mathbf{0}$, and $\mathbf{f}_y(t) = \mathbf{0}$, it can be shown that the dynamics of the state estimation error become

$$\mathbf{e}_x^i(t+1) = \mathbf{F}^i \mathbf{e}_x^i(t) + (\mathbf{F}^i \mathbf{T}^i - \mathbf{T}^i \mathbf{A} + \mathbf{S}^i \mathbf{C}) \mathbf{x}(t) + (\mathbf{J}^i - \mathbf{T}^i \mathbf{B}) \mathbf{u}(t) - \mathbf{T}^i \mathbf{B} \mathbf{f}_u(t),$$

whilst the residual vector is given by

$$\mathbf{r}^i(t) = \mathbf{L}_1^i \mathbf{e}_x^i(t) + (\mathbf{L}_1^i \mathbf{T}^i + \mathbf{L}_2^i \mathbf{C}) \mathbf{x}(t).$$

15/04/2011

UIO for FDI (Cont'd)

whilst the residual vector is given by

$$\mathbf{r}^i(t) = \mathbf{L}_1^i \mathbf{e}_x^i(t) + (\mathbf{L}_1^i \mathbf{T}^i + \mathbf{L}_2^i \mathbf{C}) \mathbf{x}(t).$$

It can be seen that if

$$\left. \begin{aligned} \mathbf{F}^i \mathbf{T}^i - \mathbf{T}^i \mathbf{A} + \mathbf{S}^i \mathbf{C} &= \mathbf{0}, \\ \mathbf{J}^i &= \mathbf{T}^i \mathbf{B}, \\ \mathbf{L}_1^i \mathbf{T}^i + \mathbf{L}_2^i \mathbf{C} &= \mathbf{0}, \end{aligned} \right\}$$

UIO for input
sensor $\mathbf{f}_u(t)$
fault isolation

$$\left. \begin{aligned} \mathbf{e}_x^i(t+1) &= \mathbf{F}^i \mathbf{e}_x^i(t) + \mathbf{T}^i \mathbf{B} \mathbf{f}_u(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{e}_x^i(t) \end{aligned} \right\}$$

15/04/2011

UIO for FDI (Cont'd)

$$\left. \begin{aligned} \mathbf{z}^i(t+1) &= (\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}) \mathbf{z}^i(t) + \mathbf{J}^i \mathbf{u}(t) + \mathbf{S}^i \mathbf{y}(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{z}^i(t) + \mathbf{L}_2^i \mathbf{y}(t) \end{aligned} \right\}$$

$$\left. \begin{aligned} \mathbf{e}_x^i(t+1) &= \mathbf{F}^i \mathbf{e}_x^i(t) + \mathbf{T}^i \mathbf{B} \mathbf{f}_u(t), \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{e}_x^i(t). \end{aligned} \right\}$$

If the linear transformation \mathbf{T}^i is chosen as [Chang & Hsu, 1995]

$$* \quad \mathbf{T}^i = \mathbf{I}_n - \mathbf{B}_i (\mathbf{C} \mathbf{B}_i)^+ \mathbf{C} \quad (4.25)$$

where \mathbf{B}_i is the i -th column of \mathbf{B} matrix and \mathbf{K}^i is selected such that $\mathbf{F}^i = \mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}$ is asymptotically stable, then, the solutions of Equation are obtained as

$$** \quad \left. \begin{aligned} \mathbf{F}^i &= \mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}, \\ \mathbf{S}^i &= \mathbf{K}^i + \mathbf{F}^i \mathbf{B}_i (\mathbf{C} \mathbf{B}_i)^+, \\ \mathbf{J}^i &= \mathbf{T}^i \mathbf{B}, \\ \mathbf{L}_1^i &= -\mathbf{C}, \\ \mathbf{L}_2^i &= [\mathbf{I}_m - (\mathbf{C} \mathbf{B}_i)(\mathbf{C} \mathbf{B}_i)^+]. \end{aligned} \right\} \left. \begin{aligned} \mathbf{F}^i \mathbf{T}^i - \mathbf{T}^i \mathbf{A} + \mathbf{S}^i \mathbf{C} &= \mathbf{0}, \\ \mathbf{J}^i &= \mathbf{T}^i \mathbf{B}, \\ \mathbf{L}_1^i \mathbf{T}^i + \mathbf{L}_2^i \mathbf{C} &= \mathbf{0}, \end{aligned} \right\}$$

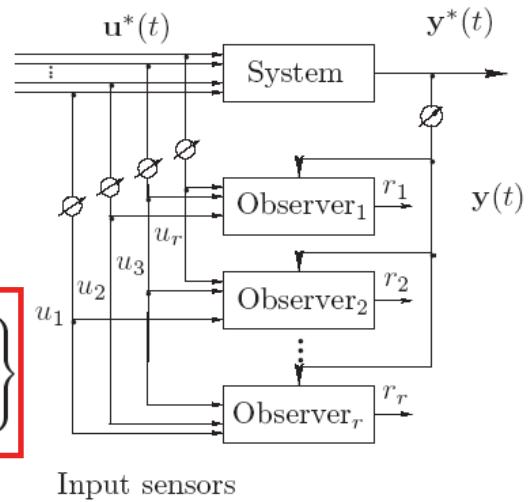
The selection of the \mathbf{B}_i matrix in Equations * and ** sets to zero the i -th column of the \mathbf{J}^i matrix. That is, the estimation error and then the residual of the i -th UIO become independent of the i -th system input.

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UIO for FDI (Cont'd)

$$\left. \begin{aligned} \mathbf{e}_x^i(t+1) &= \mathbf{F}^i \mathbf{e}_x^i(t) + \mathbf{T}^i \mathbf{B} \mathbf{f}_u(t), \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{e}_x^i(t). \end{aligned} \right\} *$$

$$\left. \begin{aligned} \mathbf{z}^i(t+1) &= (\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}) \mathbf{z}^i(t) + \mathbf{J}^i \mathbf{u}(t) + \mathbf{S}^i \mathbf{y}(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{z}^i(t) + \mathbf{L}_2^i \mathbf{y}(t) \end{aligned} \right\} **$$



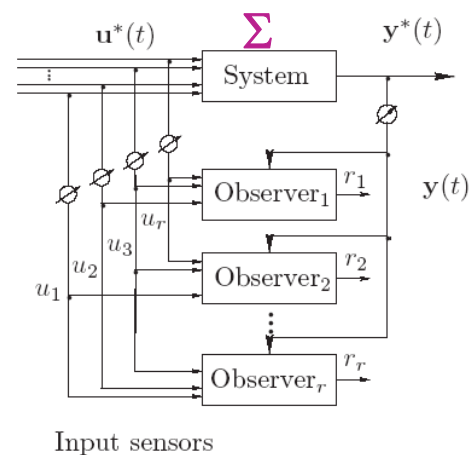
The selection of the \mathbf{B}_i matrix in Equations * and ** sets to zero the i -th column of the \mathbf{J}^i matrix. That is, the estimation error and then the residual of the i -th UIO become independent of the i -th system input.

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UIO for FDI (Cont'd)

$$\left. \begin{aligned} \mathbf{e}_x^i(t+1) &= \mathbf{F}^i \mathbf{e}_x^i(t) + \mathbf{T}^i \mathbf{B} \mathbf{f}_u(t), \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{e}_x^i(t). \end{aligned} \right\}$$

$$\left. \begin{aligned} \mathbf{z}^i(t+1) &= (\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}) \mathbf{z}^i(t) + \mathbf{J}^i \mathbf{u}(t) + \mathbf{S}^i \mathbf{y}(t) \\ \mathbf{r}^i(t) &= \mathbf{L}_1^i \mathbf{z}^i(t) + \mathbf{L}_2^i \mathbf{y}(t) \end{aligned} \right\}$$

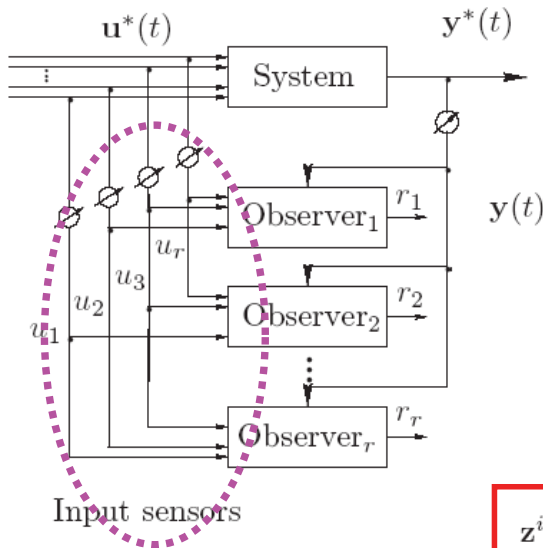


Under the hypothesis of observability of the system Σ and in the absence of input faults ($\mathbf{f}_u(t) = \mathbf{0}$), it can be seen that the i -th residual vector reaches zero as t approaches infinity and the rate of convergence depends on the position of the eigenvalues of $\mathbf{T}^i \mathbf{A} - \mathbf{K}^i \mathbf{C}$ matrix inside the unit circle.

In the presence of a fault on the i -th input, the i -th residual reaches zero asymptotically while the residuals of the $r - 1$ remaining observers are sensitive to the fault signal. This situation leads to the possibility of unique detection and isolation of all process input faults.

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Fault Isolation with UIO



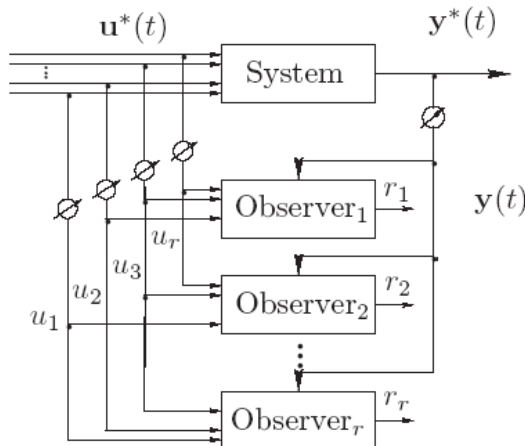
Each observer is insensitive to one input sensor:

Table 4.1: Fault signatures.

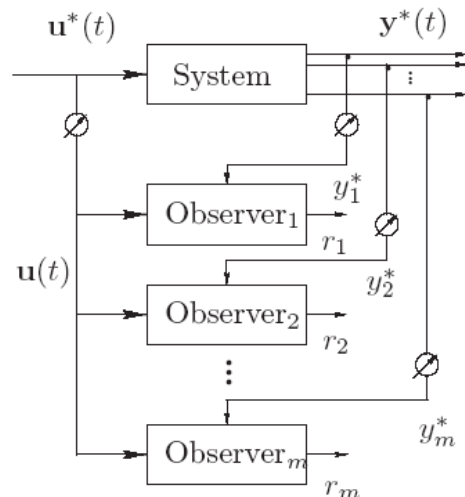
	u_1	u_2	...	u_r	y_1	y_2	...	y_m
r_{UIO_1}	0	1	...	1	1	1	...	1
r_{UIO_2}	1	0	...	1	1	1	...	1
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots
r_{UIO_r}	1	1	...	0	1	1	...	1

$$\left. \begin{aligned} z^i(t+1) &= (T^i A - K^i C)z^i(t) + J^i u(t) + S^i y(t) \\ r^i(t) &= L_1^i z^i(t) + L_2^i y(t) \end{aligned} \right\}$$

Multiple FDI



Input sensor FDI



Input sensor FDI

Multiple FDI (Cont'd)

Table 4.1: Fault signatures.

	u_1	u_2	...	u_r	y_1	y_2	...	y_m
<i>UIO</i>	r_{UIO_1}	0	1	...	1	1	...	1
	r_{UIO_2}	1	0	...	1	1	...	1

	r_{UIO_r}	1	1	...	0	1	1	...
<i>Dynamic Observers</i>	r_{O_1}	1	1	...	1	0	...	0
	r_{O_2}	1	1	...	1	0	...	0

	r_{O_m}	1	1	...	1	0	0	...

Fault Signature

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Multiple FDI (Cont'd)

Table 4.1: Fault signatures.

	u_1	u_2	...	u_r	y_1	y_2	...	y_m
r_{UIO_1}	0	1	...	1	1	1	...	1
r_{UIO_2}	1	0	...	1	1	1	...	1
...
r_{UIO_r}	1	1	...	0	1	1	...	1
r_{O_1}	1	1	...	1	1	0	...	0
r_{O_2}	1	1	...	1	0	1	...	0
...
r_{O_m}	1	1	...	1	0	0	...	1

i) The residuals which are affected by the input and output faults are described by an entry '1' in the corresponding table entry, while an entry '0' means that the input or output fault does not affect the corresponding residual.

ii) Note how multiple faults in the system outputs can be isolated since a fault on the i -th output signal affects only the residual function r_{O_i} of the output observer driven by the i -th output, but all the UIO or UIKF residual functions r_{UIO_i} . On the other hand, multiple faults on the inputs cannot be isolated by means of this technique since all the residual functions are sensitive to faults regarding different inputs.

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Residual Disturbance *Robustness*

- Residuals decoupled from disturbance
- Robust residual generator
- Disturbance effect minimisation
- Measurement errors

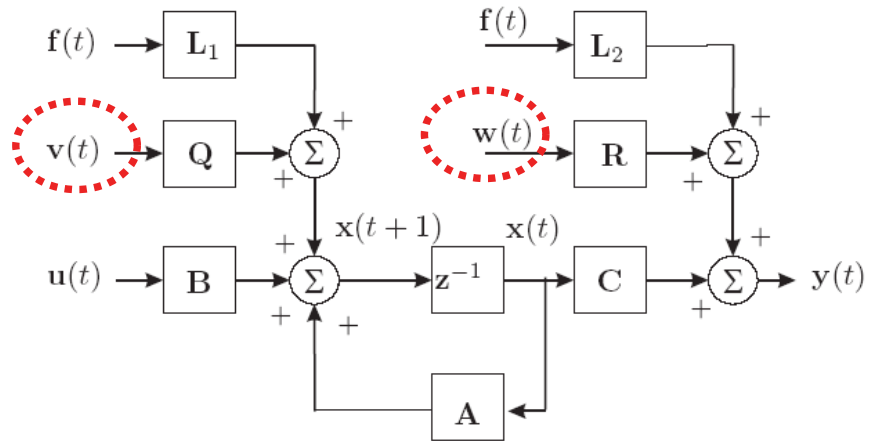


Figure 2.14: MIMO process with faults and noises.

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FDI with *Noisy Measurements*

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) + \mathbf{L}_1\mathbf{f}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) + \mathbf{L}_2\mathbf{f}(t) \end{cases}$$

✓ Model with fault and noise

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) \end{cases}$$

➤ Model with noise only: Kalman filter!

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Kalman Filter Design

$$* \begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) \end{cases}$$

With reference to the time-invariant, discrete-time, linear dynamic system described by Equation * the i -th KF for the i -th output has the structure [Jazwinski, 1970]:

$$\begin{aligned} \mathbf{x}_F^i(t+1|t) &= \mathbf{A}\mathbf{x}_F^i(t|t) + \mathbf{B}\mathbf{u}(t) \\ y_F^i(t+1|t) &= \mathbf{C}_i\mathbf{x}_F^i(t+1|t) \end{aligned}$$

(State and Output Prediction)

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Kalman Filter Design (Cont'd)

$$\begin{aligned} \mathbf{P}(t+1|t) &= \mathbf{A}\mathbf{P}(t|t)\mathbf{A}^T + \mathbf{Q} \\ \mathbf{K}_i(t+1) &= \mathbf{P}(t+1|t)\mathbf{C}_i^T [\mathbf{C}_i\mathbf{P}(t+1|t)\mathbf{C}_i^T + \mathbf{R}]^{-1} \\ \mathbf{x}_F^i(t+1|t+1) &= \mathbf{x}_F^i(t+1|t) + \mathbf{K}_i(t+1)[y_i(t+1) - \hat{y}_F^i(t+1|t)] \\ \mathbf{P}(t+1|t+1) &= [\mathbf{I} - \mathbf{K}_i(t+1)\mathbf{C}_i]\mathbf{P}(t+1|t)[\mathbf{I} - \mathbf{K}_i(t+1)\mathbf{C}_i]^T + \\ &\quad + \mathbf{K}_i(t+1)\mathbf{R}\mathbf{K}_i^T(t+1). \end{aligned}$$

(Vector Updates)

The variables $\mathbf{x}_F^i(t+1|t)$ and $y_F^i(t+1|t)$ are the one step prediction of the state and of the output of the process, respectively. $\mathbf{x}_F^i(t|t)$ is the state estimation given by the filter, \mathbf{C}_i the i -th row of the output distribution matrix \mathbf{C} , $\mathbf{P}(t+1|t)$ is the covariance matrix of the one step prediction error $\mathbf{x}(t+1) - \mathbf{x}_F^i(t+1|t)$ whilst $\mathbf{P}(t|t)$ is the covariance matrix of the filtered state error $\mathbf{x}(t) - \mathbf{x}_F^i(t|t)$.

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Kalman Filter Design (Cont'd)

$$\mathbf{P}(t+1|t) = \mathbf{A}\mathbf{P}(t|t)\mathbf{A}^T + \mathbf{Q}$$

$$\mathbf{K}_i(t+1) = \mathbf{P}(t+1|t)\mathbf{C}_i^T [\mathbf{C}_i\mathbf{P}(t+1|t)\mathbf{C}_i^T + \mathbf{R}]^{-1}$$

$$\mathbf{x}_F^i(t+1|t+1) = \mathbf{x}_F^i(t+1|t) + \mathbf{K}_i(t+1)[y_i(t+1) - \hat{y}_F^i(t+1|t)]$$

$$\mathbf{P}(t+1|t+1) = [\mathbf{I} - \mathbf{K}_i(t+1)\mathbf{C}_i]\mathbf{P}(t+1|t)[\mathbf{I} - \mathbf{K}_i(t+1)\mathbf{C}_i]^T + \mathbf{K}_i(t+1)\mathbf{R}\mathbf{K}_i^T(t+1).$$

(Vector Updates)

\mathbf{Q} is the covariance matrix of the input vector noise $\tilde{\mathbf{u}}(t)$ and \mathbf{R} is the variance of the i -th component of the output noise $\tilde{y}(t)$. $\mathbf{K}_i(t+1)$ is the time-variant gain of the filter and $y_i(t)$ is the i -th component of the measured output $y(t)$.

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) \end{cases}$$

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Kalman Filter Properties (Cont'd)

- Defined: $e(t) = x(t) - \hat{x}(t)$
 - It minimises: $E[e^T(t)e(t)] \equiv P(t)$
 - *i.e.* the mean square error & the error covariance matrix
- Filter gain $K(t)$
 - Solution of the difference equation:

$$P(t+1) = -\mathbf{A}\mathbf{P}(t)\mathbf{C}^T [\mathbf{R} + \mathbf{C}\mathbf{P}(t)\mathbf{C}^T]^{-1} \mathbf{C}\mathbf{P}(t)\mathbf{A}^T + \mathbf{A}\mathbf{P}(t)\mathbf{A} + \mathbf{Q}$$

15/04/2011

Kalman Filtering for FDI

$$* \begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) + \mathbf{L}_1\mathbf{f}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) + \mathbf{L}_2\mathbf{f}(t) \end{cases}$$

1) It can be proved that the innovation $e_i(t+1) = y_i(t+1) - y_F^i(t+1|t) = y_i(t+1) - \mathbf{C}_i \mathbf{x}_F^i(t+1|t)$ is a zero-mean white process when all the assumptions regarding the system * and the statistical characteristics of the noises described by Equation * are completely fulfilled. A Riccati equation is ob-

2) In the presence of a fault on the i -th output ($f_{y_i}(t) \neq 0$), the stochastic properties (mean-value, variance and whiteness, etc) of the innovation process $e_i(t)$ change abruptly so that the fault detection can be based on these variations [Basseville, 1988].

3) Finally, note how multiple faults in outputs can be isolated since a fault on the i -th output affects only the innovation of the KF driven by the i -th output and all the innovation of the filters with unknown input.

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Kalman Filtering for FDI (Cont'd)

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) + \mathbf{L}_1\mathbf{f}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) + \mathbf{L}_2\mathbf{f}(t) \end{cases}$$

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) \end{cases}$$

Innovation $e_i(t+1) = y_i(t+1) - y_F^i(t+1) = y_i(t+1) - \mathbf{C}_i \mathbf{x}_F^i(t+1|t)$

(i) Because of the linear property of the identified model and because of the additive effect of the faults on the system, it may easily be shown that the effect of the change on the innovation is also additive.

(ii) Any abrupt change in measurements due to a fault is reflected in a change in the mean value and in the standard deviation of innovations.

15/04/2011

Kalman Filtering for FDI (Cont'd)

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) + \mathbf{L}_1\mathbf{f}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) + \mathbf{L}_2\mathbf{f}(t) \end{cases}$$

$$\begin{cases} \mathbf{x}(t+1) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{Q}\mathbf{v}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{R}\mathbf{w}(t) \end{cases}$$

Innovation $e_i(t+1) = y_i(t+1) - y_F^i(t+1) = y_i(t+1) - C_i x_F^i(t+1|t)$

In particular, since the KF produces zero-mean and independent white residuals with the system in normal operation, a method for FDI consists of testing

how much the sequence of innovations has deviated from the white noise hypothesis.

15/04/2011

KF Residual Evaluation...

Which thresholds???

$$\begin{cases} J(\mathbf{r}(t)) \leq \varepsilon(t) & \text{for } \mathbf{f}(t) = \mathbf{0} \\ J(\mathbf{r}(t)) > \varepsilon(t) & \text{for } \mathbf{f}(t) \neq \mathbf{0} \end{cases}$$

Innovation $e_i(t+1) = y_i(t+1) - y_F^i(t+1) = y_i(t+1) - C_i x_F^i(t+1|t)$

15/04/2011

Kalman Filtering for FDI (Cont'd)

$$r(t) \equiv e_i(t+1) = y_i(t+1) - y_F^i(t+1) = y_i(t+1) - C_i x_F^i(t+1|t)$$

*Innovation or
Residual $r(t)$*

(i) Statistical Tests

Zero-mean

$$\bar{r}(t) = E[r(t)] = \frac{1}{t} \sum_{j=1}^t r(j)$$

&

variance

$$\sigma_r^2(t) = E[r^2(t)] = \frac{1}{t} \sum_{j=1}^t r^2(j)$$

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Kalman Filtering for FDI (Cont'd)

$$r(t) \equiv e_i(t+1) = y_i(t+1) - y_F^i(t+1) = y_i(t+1) - C_i x_F^i(t+1|t)$$

*Innovation or
Residual $r(t)$*

(ii) Statistical Tests

Whiteness test

$$R_r^t(\tau) = \frac{1}{t} \sum_{j=1}^t r(j)r(j+\tau),$$

χ^2 - type

$$\zeta_r^M(t) = \frac{t}{R_r^t(0)^2} \sum_{\tau=1}^M (R_r^t(\tau))^2$$

which are computed in a growing window. The parameter $\zeta_r^M(t)$ is a chi-squared random variable with M degrees of freedom.

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Kalman Filtering for FDI (Cont'd)

Whiteness test

$$R_r^t(\tau) = \frac{1}{t} \sum_{j=1}^t r(j)r(j+\tau),$$

χ^2 - type

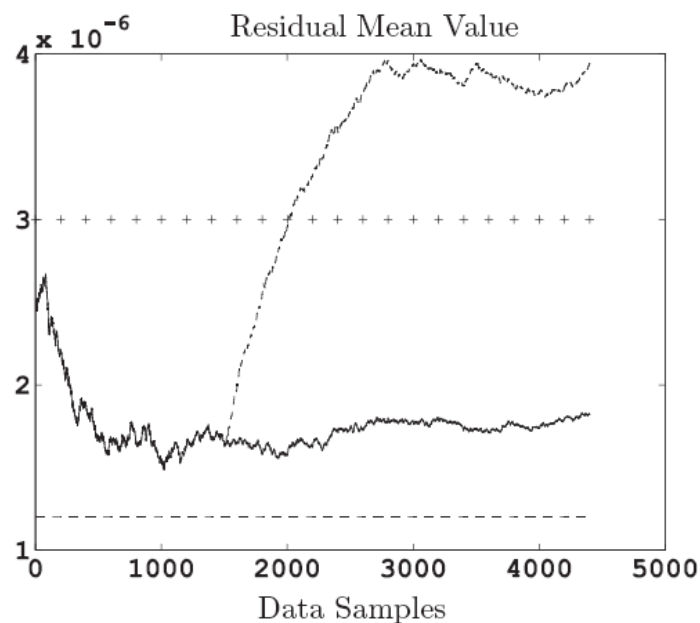
$$\zeta_r^M(t) = \frac{t}{R_r^t(0)^2} \sum_{\tau=1}^M (R_r^t(\tau))^2$$

If a system abnormality occurs, the statistics of $r(t)$ change, so the comparison of $\bar{r}(t)$ and $\zeta_r^M(t)$ with a threshold ϵ fixed under no faults conditions, becomes the detection rule 2.17. In particular, such a threshold can be settled as previously seen or, with the aid of chi-squared tables, $\epsilon = \chi_{\beta}^2(M)$ can be computed as a function of the false-alarms probability β and of the window size M .

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KF Residuals: Mean-value (example)

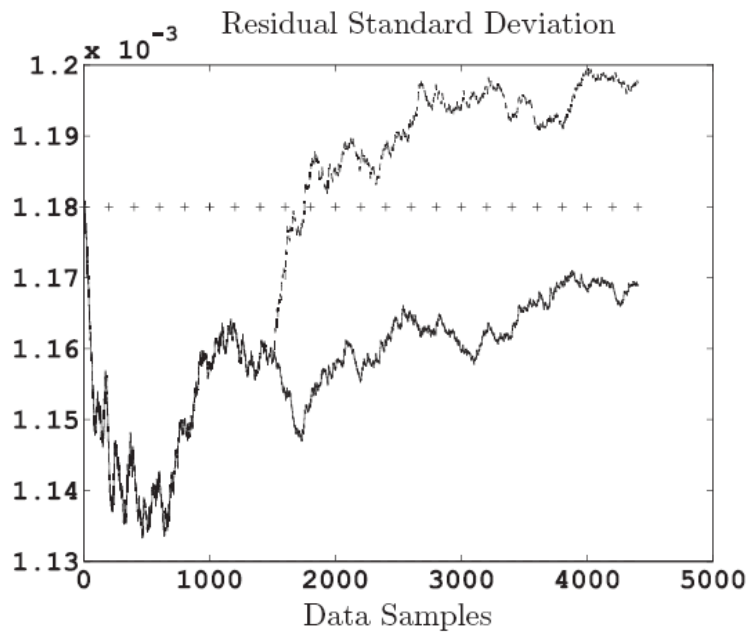
*Fault-free
&
faulty
residuals*



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KF Residuals: Standard deviation (example)

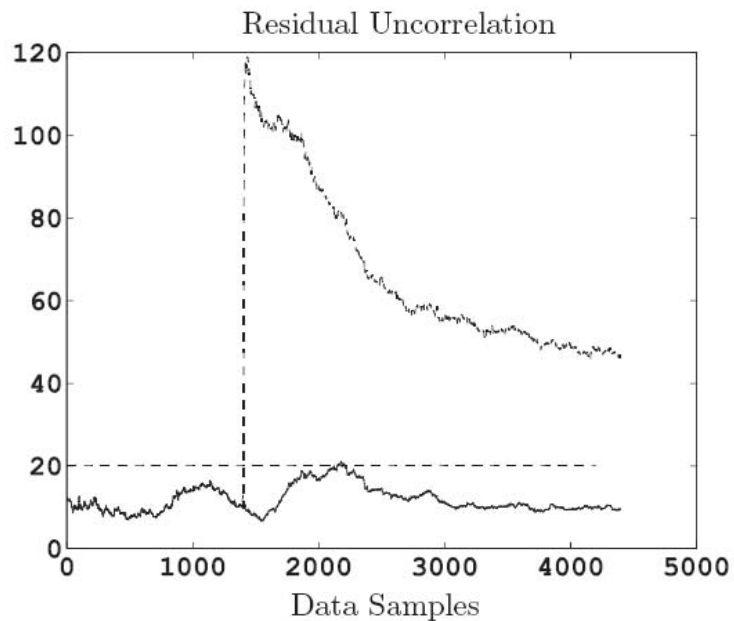
*Fault-free
&
faulty
residuals*



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KF Residuals: Whiteness test (example)

*Fault-free
&
faulty
residuals*



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Fault Detection with Parity Equations

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Parity Relations for Fault Detection

- The basic idea of the parity relations approach is to provide a proper check of the parity (consistency) of the measurements acquired from the monitored system
- In the early development of fault diagnosis, the parity vector (relation) approach was applied to static or parallel redundancy schemes, which may be obtained directly from measurements (hardware redundancy) or from analytical relations (analytical redundancy)

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Parity Relations for Fault Detection

- In the case of hardware redundancy, two methods can be exploited to obtain redundant relations
- The first requires the use of several sensors having identical or similar functions to measure the same variable
- The second approach consists of dissimilar sensors to measure different variables but with their outputs being relative to each other
- **Analytical forms of redundancy**

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Analytical Redundancy

- Model (M) and process (P)

$$G_M(z) = \frac{\hat{A}(z)}{\hat{B}(z)} \quad G_P(z) = \frac{A(z)}{B(z)}$$

- Error vector

$$r(z) = \left(\frac{A(z)}{B(z)} - \frac{\hat{A}(z)}{\hat{B}(z)} \right) u(z)$$

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Analytical Redundancy (Cont'd)

- Model (M) and process (P)

$$G_M(z) = \frac{\hat{A}(z)}{\hat{B}(z)} \quad G_P(z) = \frac{A(z)}{B(z)}$$

- Error vector

$$r(z) = \left(\frac{A(z)}{B(z)} - \frac{\hat{A}(z)}{\hat{B}(z)} \right) u(z)$$

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Analytical Redundancy (EE)

- Models, if:

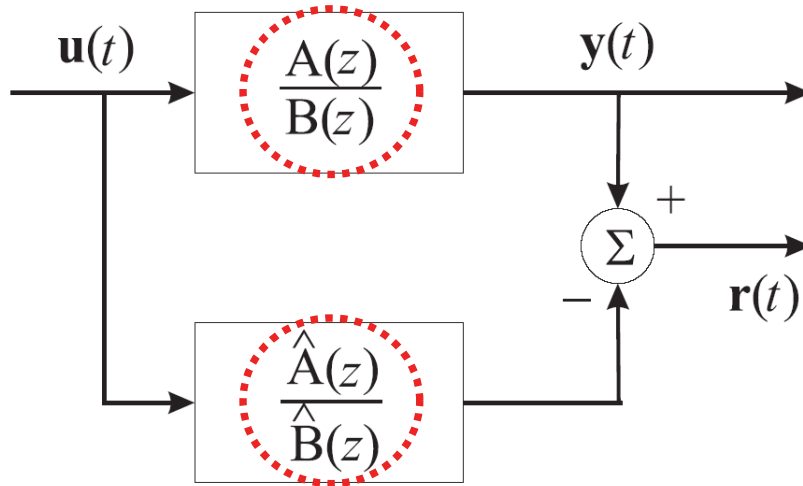
$$G_M(z) = G_P(z) \text{ i.e. } \frac{\hat{A}(z)}{\hat{B}(z)} = \frac{A(z)}{B(z)}$$

- Residual, with input and output faults

$$r(z) = \frac{A(z)}{B(z)} f_u(z) + f_y(z)$$

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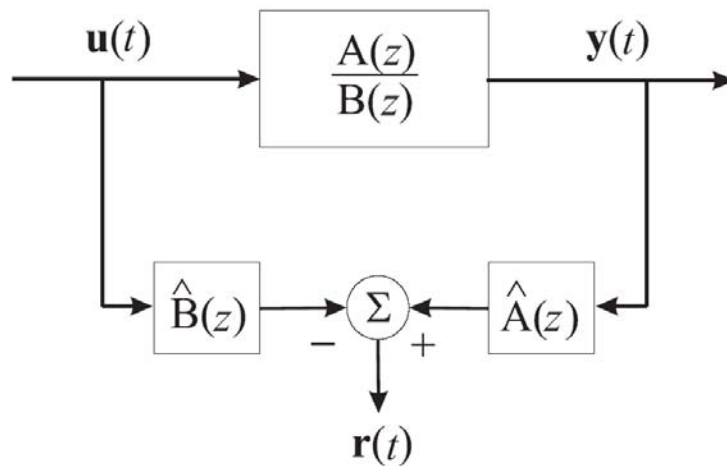
Analytical Redundancy (OE)



(a) Output error

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Parity Relation (EE)



(b) Equation error

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Parity Relations via **EE**

- According to EE, another possibility for generating a polynomial error:

$$\begin{aligned} r(z) &= \hat{A}(z)y(z) - \hat{B}(z)u(z) \\ &= B(z)f_u(z) + A(z)f_y(z) \end{aligned}$$

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Parity Relations

- The previous equations that generate residuals and are called parity equations under the assumptions of fault occurrence and of exact agreement between process and model
- However, within the parity equations, the model parameters are assumed to be known and constant, whereas the **parameter estimations** can vary the parameters of the polynomials in order to minimise the residuals

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Change Detection and Symptom Evaluation

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Residual Evaluation

- When the residual generation stage has been performed, the second step requires the examination of symptoms in order to determine if any faults have occurred
- A decision process may consist of a simple threshold test on the instantaneous values of moving averages of residuals

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Residual Evaluation (Cont'd)

- On the other hand, because of the presence of noise, disturbances and other unknown signals acting upon the monitored system, the decision making process can exploits statistical methods
- In this case, the measured or estimated quantities, such as signals, parameters, state variables or residuals are usually represented by stochastic variables

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Residual Evaluation (Cont'd)

- Mean and standard values

$$\bar{r}_i = E\{r_i(t)\}; \quad \bar{\sigma}_i^2 = E\{[r_i(t) - \bar{r}_i]^2\}$$

- Residuals or symptoms

$$\Delta r_i = E\{r_i(t) - \bar{r}_i\}; \quad \Delta \sigma_i = E\{\sigma_i(t) - \bar{\sigma}_i\}$$

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Residual Evaluation (Cont'd)

- Fixed threshold selection

$$\Delta r_{tol} = \epsilon \bar{\sigma}_r, \quad \epsilon \geq 2$$

- By a proper choice of ϵ , a compromise has to be made between the detection of small faults and false alarms
- More complex residual evaluation schemes

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Residual Generation Problem

- **Robustness issues!**
- Two design principles:
 - Uncertainty is taken into account at the residual design stage: **active robustness in fault diagnosis**
 - **Passive robustness** makes use of a residual evaluator with proper threshold selection methods (fixed or adaptive)

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Fault Diagnosis Technique Integration

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FDI Technique Integration

- Several FDI techniques have been developed and their application shows different properties with respect of the diagnosis of different faults in a process
- To achieve a reliable FDI technique, a good solution consists of a proper integration of several methods which take advantages of the different procedures
- Exploit a knowledge-based treatment of all available analytical and heuristic information

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Fuzzy Logic for Residual Generation

- Classical fault diagnosis model-based methods can exploit state-space of input-output dynamic models of the process under investigation
- Faults are supposed to appear as changes on the system state or output caused by malfunctions of the components as well as of the sensors
- The main problem with these techniques is that the precision of the process model affects the accuracy of the detection and isolation system as well as the diagnostic sensitivity

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Fuzzy Logic for Residual Generation (Cont'd)

- The majority of real industrial processes are nonlinear and cannot be modelled by using a single model for all operating conditions
- Since a mathematical model is a description of system behaviour, accurate modelling for a complex nonlinear system is very difficult to achieve in practice
- Sometimes for some nonlinear systems, it can be impossible to describe them by analytical equations

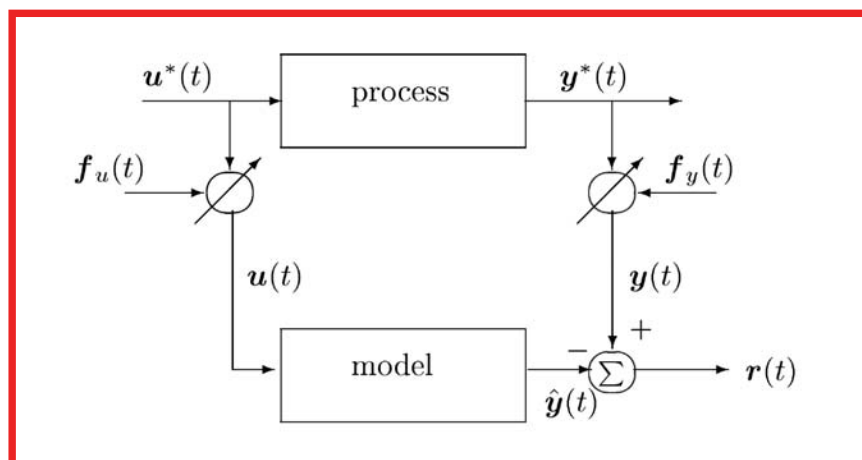
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Fuzzy Logic for Residual Generation (Cont'd)

- Sometimes the system structure or parameters are not precisely known and if diagnosis has to be based primarily on heuristic information, no qualitative model can be set up
- Because of these assumptions, fuzzy system theory seems to be a natural tool to handle complicated and uncertain conditions
- Instead of exploiting complicated nonlinear models, it is also possible to describe the plant by a collection of local affine fuzzy models, whose parameters are obtained by identification procedures

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Residual Generation via Fuzzy Models



Residual signals: $r(t) = y(t) - \hat{y}(t)$.

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Neural Networks in Fault Diagnosis

- Quantitative model-based fault diagnosis generates symptoms on the basis of the analytical knowledge of the process under investigation
- In most cases this does not provide enough information to perform an efficient FDI, *i.e.*, to indicate the location and the mode of the fault
- A typical integrated fault diagnosis system uses both analytical and heuristic knowledge of the monitored system

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Neural Networks in Fault Diagnosis (Cont'd)

- The knowledge can be processed in terms of residual generation (analytical knowledge) and feature extraction (heuristic knowledge)
- The processed knowledge is then provided to an inference mechanism which can comprise residual evaluation, symptom observation and pattern recognition

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Neural Networks in Fault Diagnosis (Cont'd)

- In recent years, neural networks (NN) have been used successfully in pattern recognition as well as system identification, and they have been proposed as a possible technique for fault diagnosis, too
- NN can handle nonlinear behaviour and partially known process because they learn the diagnostic requirements by means of the information of the training data

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Neural Networks in Fault Diagnosis (Cont'd)

- NN are noise tolerant and their ability to generalise the knowledge as well as to adapt during use are extremely interesting properties
- FDI is performed by a NN using input and output measurements
 - NN is trained to identify the fault from measurement patterns
 - Classification of individual measurement pattern is not always unique in dynamic situations, therefore the straightforward use of NN in
- Fault diagnosis of dynamic plant is not practical and other approaches should be investigated

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Neural Networks in Fault Diagnosis (Cont'd)

- A NN could be exploited in order to find a dynamic model of the monitored system or connections from faults to residuals
- In the latter case, the NN is used as pattern classifier or nonlinear function approximator
- NN are capable of approximating a large class of functions for fault diagnosis of an industrial plant
- The identification of models for the system under diagnosis as well as the application of NN as function approximator will be shown

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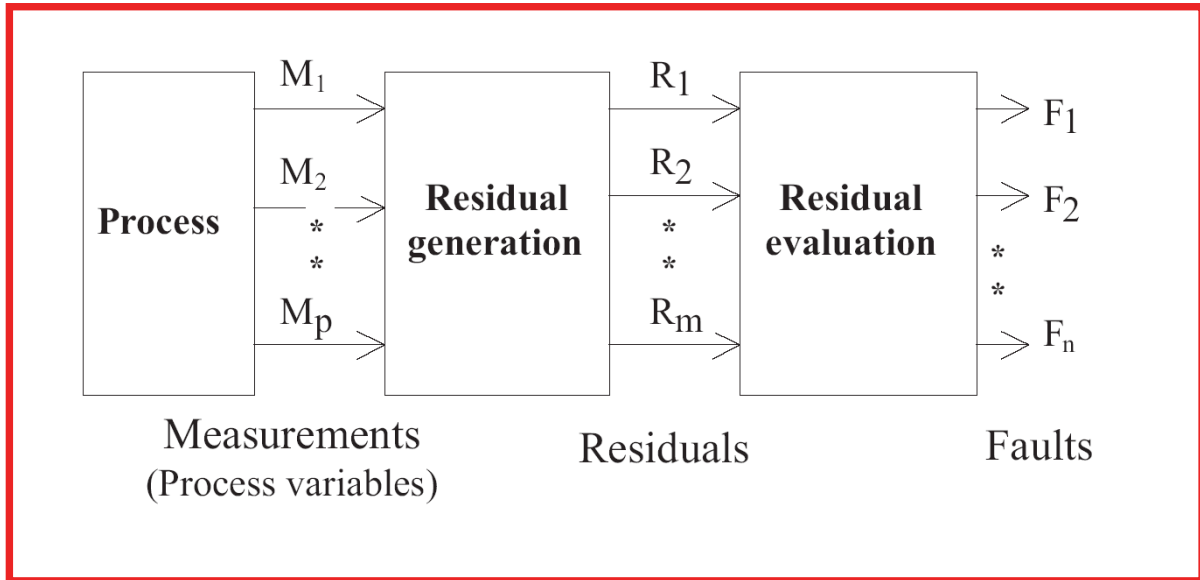


Neural Networks in Fault Diagnosis (Cont'd)

- Quantitative and qualitative approaches have a lot of complementary characteristics which can be suitably combined together to exploit their advantages and to increase the robustness of quantitative techniques
- Partial knowledge deriving from qualitative reasoning is reduced by quantitative methods
- Further research on model-based fault diagnosis consists of finding the way to properly combine these two approaches together to provide highly reliable diagnostic information

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FDI with Neural Networks



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FDI with Neural Networks (Cont'd)

- As described in the figure, the fault diagnosis methodology consists of 2 stages
- In 1st stage, the fault has to be detected on the basis of residuals generated from a bank of output estimators, while, in the 2nd step, fault identification is obtained from pattern recognition techniques implemented via NN
- Fault identification represents the problem of the estimation of the size of faults occurring in a dynamic system

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FDI with Neural Networks (Cont'd)

- A NN is exploited to find the connection from a particular fault regarding system inputs and output measurements to a particular residual
- The output predictor generates a residual which does not depend on the dynamic characteristics of the plant, but only on faults
- NNs classify static patterns of residuals, which are uniquely related to particular fault conditions independently from the plant dynamics

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FDI with Neural Networks (Cont'd)

- NNs have been used both as predictor of dynamic models for fault diagnosis, and pattern classifiers for fault identification
- The most frequently applied neural models are the feed-forward perceptron used in multi-layer networks with static structure
- The introduction of explicit dynamics requires the feedback of some outputs through time delay units

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FDI with Neural Networks (Cont'd)

- Alternatively to static structure, NN with neurons having intrinsic dynamic properties can be used
- On the other hand, NN can be effectively exploited for residual signal processing, which is actually a static pattern recognition problem

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FDI with Neural Networks (Cont'd)

- Fault signals create changes in several residuals obtained by using output predictors of the process under examination
- A neural network is exploited in order to find the connection from a particular fault regarding input and output measurements to a particular residual

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FDI with Neural Networks (Cont'd)

- The predictors generate residuals independent of the dynamic characteristics of the plant and dependent only on sensors faults
- Therefore, the neural network evaluates static patterns of residuals, which are uniquely related to particular fault conditions independently from the plant dynamics

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Conclusion – Lecture 1

- ✓ Model-Based FDI
- ✓ Analytical Redundancy
- ✓ State-Space Models
- ✓ Residual Generation
 - ✓ Unknown Input Observers UIO
 - ✓ Dynamic Observers / Kalman Filters
- ✓ Residual Evaluation/Change Detection

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